# Progress and plans for coupling continuum kinetics to M3D-C1

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# DK4D<sup>1</sup> is a time-dependent, axisymmetric drift-kinetic equation (DKE) solver

- DK4D developed for purpose of extended-MHD coupling
  - Solves non-Maxwellian part of distribution function
  - Linearized Fokker-Planck-Landau collision operators
  - Chapman-Enskog-like formulation

### Encouraging initial results

- Benchmarked to Sauter model, along with NIMROD, NCLASS, and NEO codes<sup>2</sup>
- Coupling to reduced MHD code produced self-consistent simulations of dynamic bootstrap current formation<sup>3</sup>



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ERAL ATOM

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<sup>3</sup>B.C. Lyons. Doctoral dissertation. Princeton University 2014. Bootstrap current evolution during slow & fast ELM-like pressure collapses



#### • Complex, linear 2D

- Must solve new DKE driven by linear MHD perturbations
- Provides drift-kinetic corrections to linear stability (e.g., RWM)

### Real, nonlinear 2D

- Must solve heat flux instability
- Provides neoclassical transport for steady-state equilibria

### Nonlinear 3D

- Must solve 5D version of Ramos DKEs
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# Modifications to DK4D would allow linear stability analysis of resistive wall modes

### New coupled drift-kinetic MHD formulation derived by Ramos

- Chapman-Enskog-like for self-consistency
- Fokker-Planck-Landau collisions
- Rotation of order the sound speed
- Two-fluid effects
- Zero-Larmor-radius limit

### Linearized about

- Axisymmetric, single-fluid, collisionless equilibrium
- Maxwellian distribution function

### Linear solution evolves time-dependently

- n=0 perturbation which corrects assumed equilibrium
- Single toroidal harmonic for stability analysis





## New DKE has similar structure to the one already implemented in DK4D

DK4D

New

$$\begin{split} \frac{\partial \bar{f}_{NMs}}{\partial t} + wy\mathbf{b}\cdot\nabla\bar{f}_{NMs} - \frac{1}{2}w\left(1-y^2\right)\mathbf{b}\cdot\nabla\ln B\frac{\partial \bar{f}_{NMs}}{\partial y} &= \langle C_{ss} + C_{ss'} \rangle_{\alpha} \\ &+ \left\{\frac{wy}{nT_s} \left[\frac{2}{3}\mathbf{b}\cdot\nabla\left(p_{s\parallel} - p_{s\perp}\right) - \left(p_{s\parallel} - p_{s\perp}\right)\mathbf{b}\cdot\nabla\ln B - \mathbf{b}\cdot\mathbf{F}_s^{coll}\right] \\ &+ P_2(y)\frac{w^2}{3v_{ths}^2}\left(\nabla\cdot\mathbf{u}_s - 3\mathbf{b}\cdot\left[\mathbf{b}\cdot\nabla\mathbf{u}_s\right]\right) + \frac{1}{3nT_s}\left(\frac{w^2}{v_{ths}^2} - 3\right)\nabla\cdot\left(q_{s\parallel}\mathbf{b}\right) \\ &- \frac{\varsigma\left(e_s\right)I}{3m_s\Omega_s}\left[\frac{1}{2}P_2(y)\frac{w^2}{v_{ths}^2}\left(\frac{w^2}{v_{ths}^2} - 5\right) + \frac{w^4}{v_{ths}^4} - 10\frac{w^2}{v_{ths}^2} + 15\right]\mathbf{b}\cdot\nabla\ln B\frac{dT_s}{d\psi}\right\}f_{Ms} \\ &\frac{\partial \bar{f}_{s1}}{\partial t} + (\mathbf{u}_0 + w_{\parallel}\mathbf{b}_0)\cdot\frac{\partial \bar{f}_{s1}}{\partial \mathbf{x}} + \frac{\mathbf{b}_0}{m_s}\cdot\left(T_{s0}\nabla\ln n_0 + e_s\eta_{cl0}\mathbf{j}_0\right)\frac{\partial \bar{f}_{s1}}{\partial w_{\parallel}} + \frac{w_{\perp}}{2}\left(\mathbf{b}_0\cdot\nabla\ln B_0\right)\left(w_{\parallel}\frac{\partial \bar{f}_{s1}}{\partial w_{\perp}} - w_{\perp}\frac{\partial \bar{f}_{s1}}{\partial w_{\parallel}}\right) = \\ &= \left\{-\left[\mathbf{u}_{s1} + \frac{n_1}{n_0}w_{\parallel}\mathbf{b}_0\right]\cdot\nabla\ln n_0 + \left[\left(\frac{3}{2} - \frac{m_sw^2}{2T_{s0}}\right)\mathbf{u}_{s1} + \left(\frac{5}{2} - \frac{m_sw^2}{2T_{s0}}\right)\frac{w_{\parallel}}{B_0}\mathbf{B}_1\right]\cdot\nabla\ln T_{s0} + \\ &+ \frac{w_{\parallel}}{n_0T_{s0}}\mathbf{b}_0\cdot\left[\nabla p_{s\parallel 1} - \left(p_{s\parallel 1} - p_{s\perp 1}\right)\nabla\ln B_0 + e_s(n_0 - n_1)\eta_{cl0}\mathbf{j}_0 - \mathbf{F}_{s1}^{coll}\right] + \frac{e_s\eta_{cl0}w_{\parallel}}{B_0T_{s0}}\left(\mathbf{B}_1 - B_1\mathbf{b}_0\right)\cdot\mathbf{j}_0 - \\ &- \frac{m_s}{2T_{s0}}\left[w_{\perp}^2\nabla\cdot\mathbf{u}_{s1} + \left(2w_{\parallel}^2 - w_{\perp}^2\right)\left(\mathbf{b}_0\mathbf{b}_0\right):\left(\nabla\mathbf{u}_{s1}\right) + \left(\frac{2w_{\parallel}^2 - w_{\perp}^2}{B_0}\right)\left(\mathbf{b}_0\mathbf{B}_1 + \mathbf{B}_1\mathbf{b}_0\right):\left(\nabla\mathbf{u}_{s0}\right)\right\}f_{Ms0} + \\ &+ \sum_{s'}\left(C_{ss'}[f_{Ms0}, f_{Ms'0}] + C_{ss'}[f_{Ms0}, \bar{f}_{s'1}] + C_{ss'}[\bar{f}_{s1}, f_{Ms'0}]\right) \end{split}$$

GENERAL ATOMICS

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### Development of DK4D & M3D-C1 required

- DK4D
  - Expand new DKE in DK4D variables and representations
  - Change to complex variables for linear stability analysis (e<sup>inφ</sup>)
  - Ax=B system
    - A will require some modification, but much can be reused
    - **B** will be redone completely for new source terms
- M3D-C1
  - Add new closure terms based on moments of drift-kinetic solution
  - Calculate equilibria in flux coordinates
  - Fast evolution of instability must be treated carefully
- Codes will likely need to be compiled together and run simultaneously
  - Both codes would be linear
  - Reuse matrices and LU decompositions for maximum efficiency



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### Implicit heat flux causes instability in DK4D

- B ·∇T should develop if q // does not have the Pfrisch-Schulter-like component
- Should require tight coupling to temperature equation
  - Without: exponential growth
  - With: oscillatory, but exponential
- Unclear if the coupled system is still missing physics or, more likely, there's a numerical instability



# Coupling M3D-C1 & axisymmetric DK4D would permit realistic transport-timescale simulations

- M3D-C1 can calculate steady-state, axisymmetric equilibria
  - Sources included in two-fluid MHD equations (e.g., particle source)
  - Transport model assumed (Spitzer resistivity, Braginskii pressure tensor)
  - Evolve to steady-state to predict axisymmetric equilibria (e.g. NSTX<sup>1</sup>)
- DK4D would provide neoclassical transport model
  - Friction force and pressure anisotropy close momentum equations
  - Parallel heat flux closes temperature equation (if needed)
  - Self-consistent neoclassical resistivity and bootstrap current would develop
- Code development has some similarity to linear stability work

<sup>1</sup>Ferraro, N.M. and S.C. Jardin. J. Comput. Phys. 228 (2009) 7742–7770.



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# Full finite-element representation may be superior to DK4D's mixed representation

- DK4D uses Legendre polynomials in  $y = \cos \chi$  and Fourier modes in  $\theta$
- Finite elements could improve resolution of trapped-passing boundary
  - Triangular mesh in y and  $\theta$
  - Adaptive packing along TPB
  - Used in M3D-C<sup>1</sup> to resolve resistive layers at rational surfaces

### Could be some difficulties

- Requires unstructured and periodic mesh
- Denser matrices, particularly with implicit moments





# Full, non-axisymmetric geometries would require substantial upgrades to DK4D

- Can no longer assume good, nested flux surfaces
  - Important effects in and around magnetic islands
  - Flux tubes could replace flux surfaces, allowing for extensive parallelization
- Must determine best representation in toroidal angle
  - Fourier modes may be simplest to implement
  - Maybe finite elements if also implemented for y and  $\theta$ ?
- Close collaboration with ASCR colleagues likely required

