

Update on Disruption-Mitigation Research at GA

by

B.C. Lyons¹, C.C. Kim², J. McClenaghan¹, P.B. Parks¹, L.L. Lao¹

¹ General Atomics

² SLS2 Consulting

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M3D-C1 Impurity-MHD Modeling

B.C. Lyons, N.M. Ferraro, S.C. Jardin

M3D-C1 Extended-MHD Solver Coupled to KPRAD

- **M3D-C1* solves the extended-MHD equations**
 - 3D toroidal geometry
 - Full (not reduced) MHD
 - High-order finite-element representation in (R, ϕ, Z)
 - Two-fluid effects (optional)
 - Finite-thickness resistive wall (optional)
- **Recently coupled[†] to KPRAD[‡] for impurity-plasma interactions**
 - Coronal (non-equilibrium) model
 - Impurity charge states and electron density evolve according to ionization and recombination
 - Thermal energy loss (ionization and radiation) coupled to
 - One (total) or two (total & electron) pressure equations
 - One (all-species) or two (all-ion and electron) temperature equations
 - Subcycled much faster than typical MHD time steps

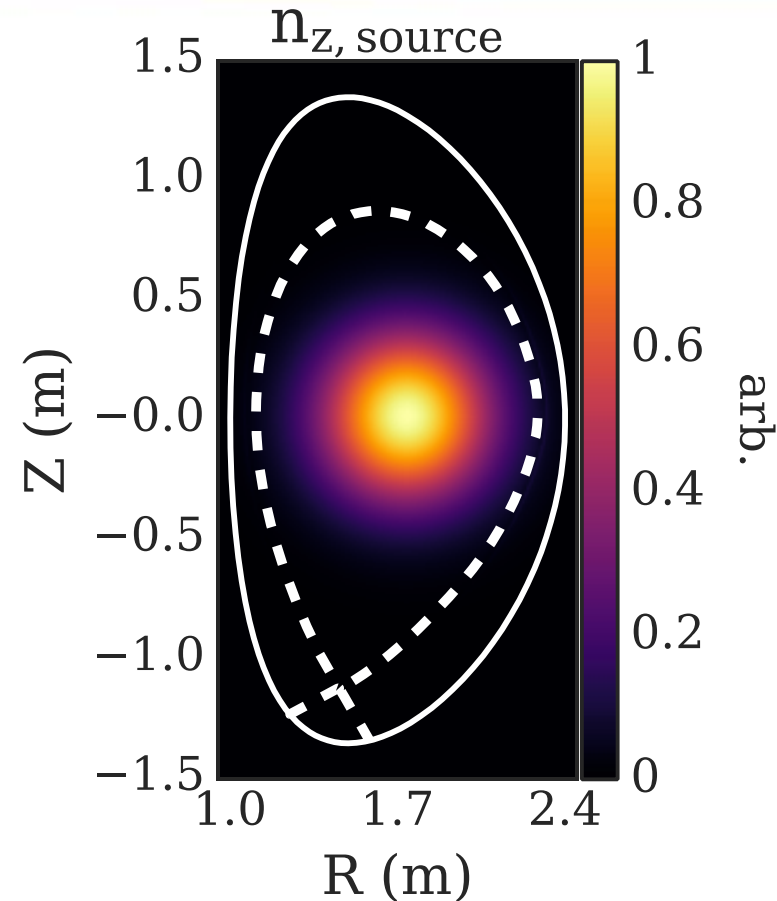
* S. C. Jardin, et al., *Comput. Sci. Discovery* 5, 014002 (2012).

† N.M. Ferraro et al. *Nucl. Fusion* 59 016001 (2019).

‡ D.G. Whyte, et al., *Proc. of the 24th Euro. Conf. on Controlled Fusion and Plasma Physics*, Vol. 21A, p. 1137 (1997).

M3D-C1 and NIMROD* Coupling to KPRAD Successfully Benchmarked in Axisymmetric Simulations †

- **Both codes solved same problem of impurity injection into DIII-D core**
 - DIII-D shot 137611 @ 1950 ms
 - 2D, nonlinear, single-fluid
 - Single-temperature equation
 - Fixed boundary
 - Constant injection of neutrals in Gaussian centered on-axis
- **Quantitative agreement found in**
 - 0D time histories
 - 2D contours
 - Temperature
 - Current



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doi.org/10.1088/1361-6587/ab0e42

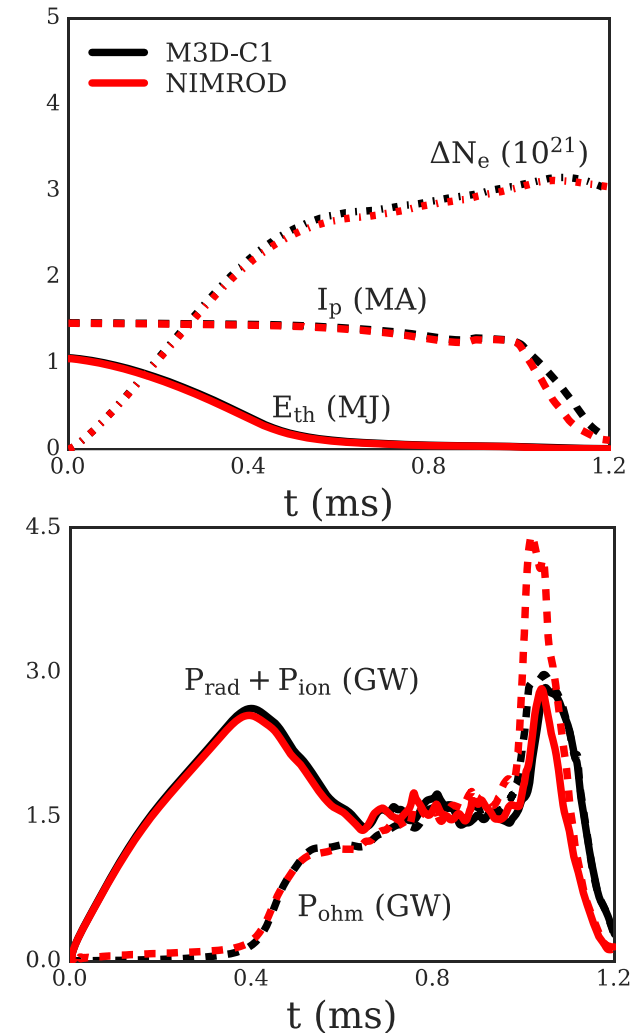
*C. R. Sovinec et al., J. Comput. Phys. 195, 355 (2004).
C. Sovinec & J. King, J. Comput. Phys. 229, 5803 (2010).

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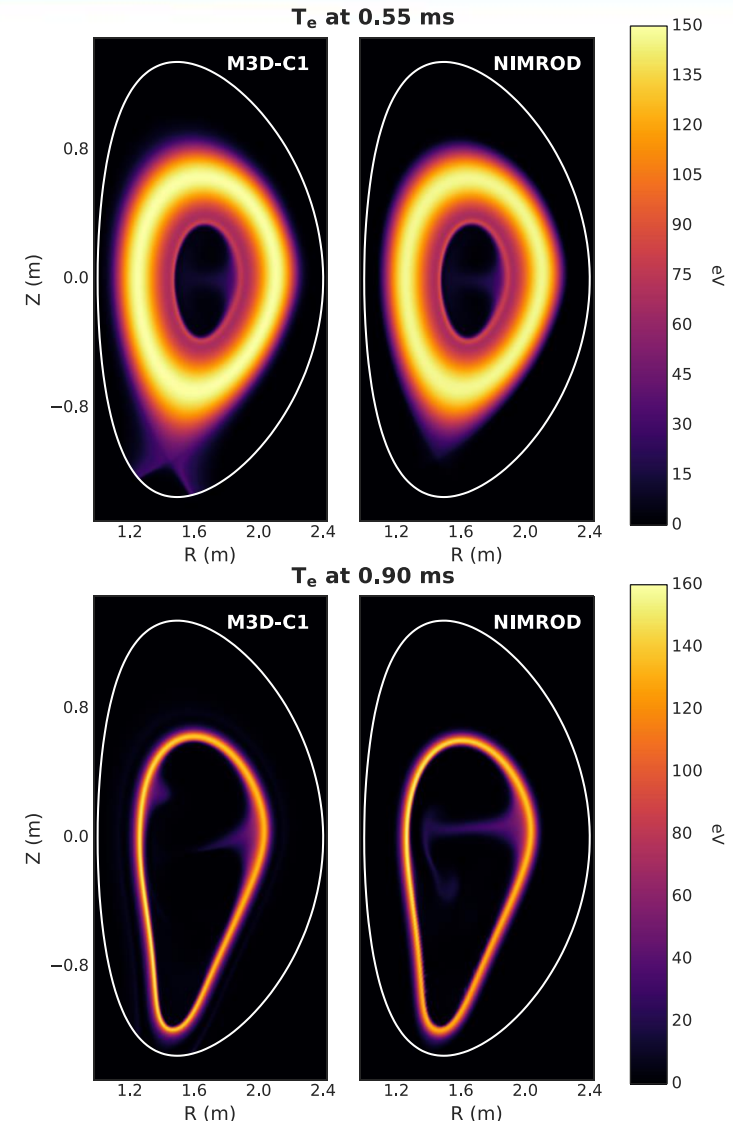
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Argon injection



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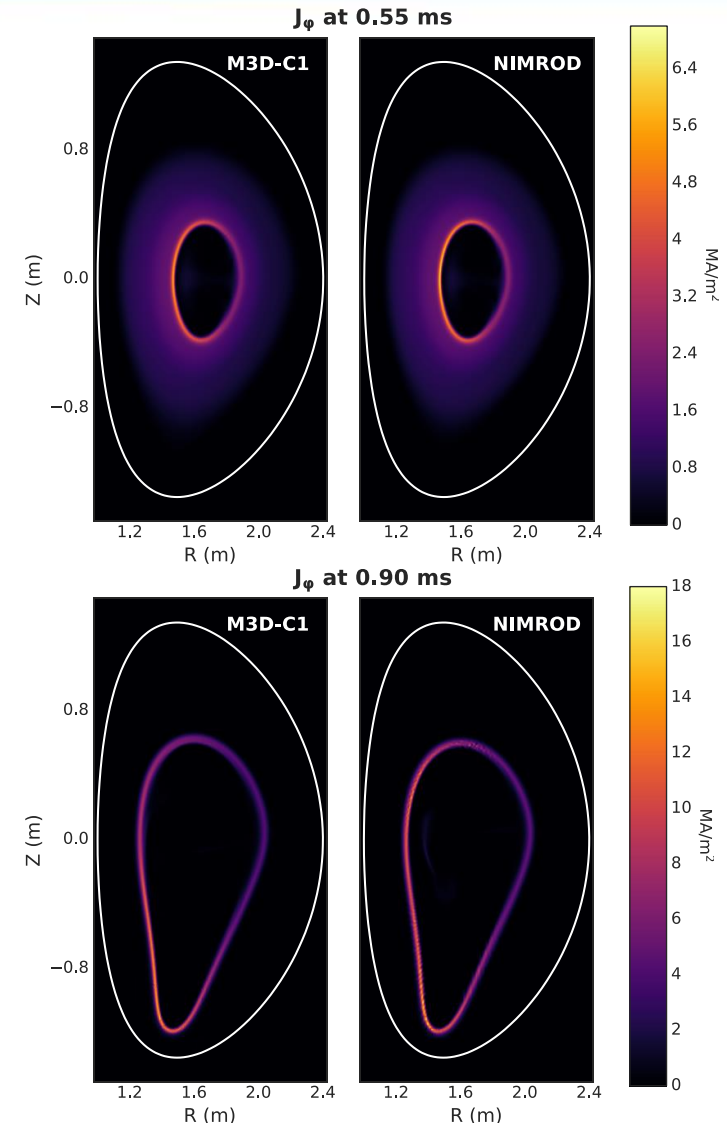
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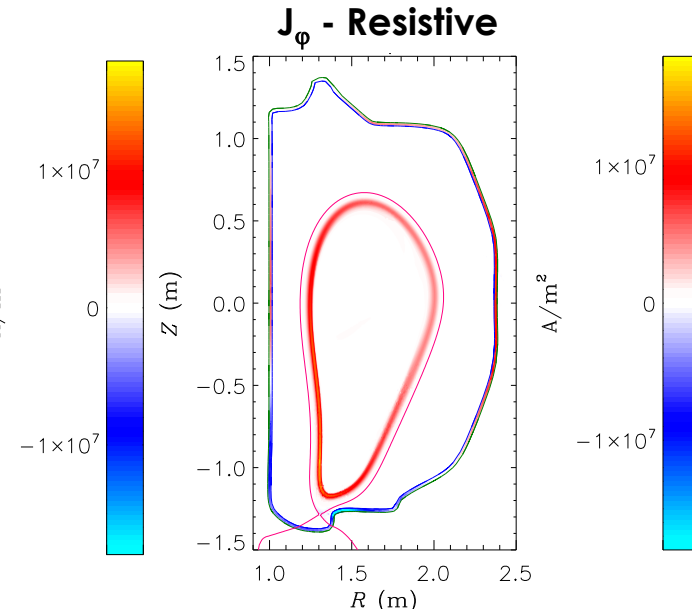
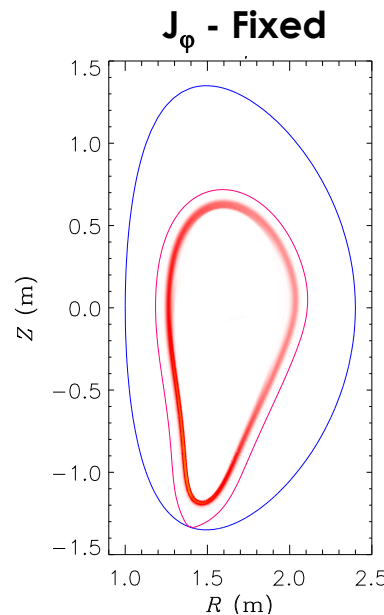
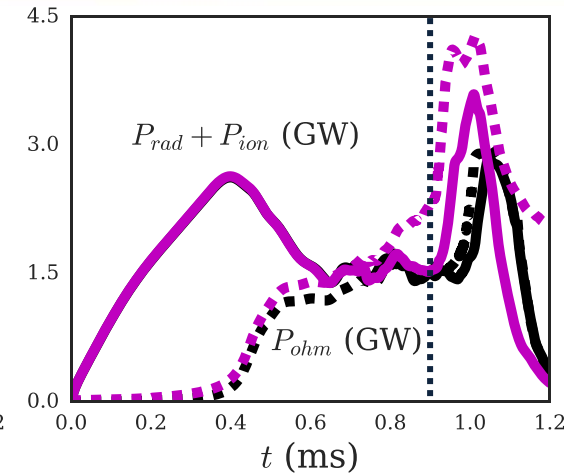
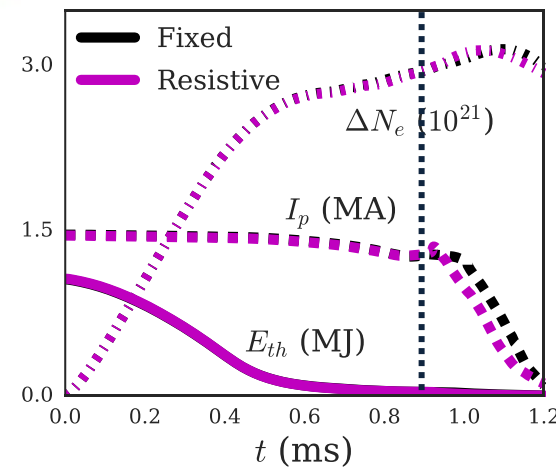
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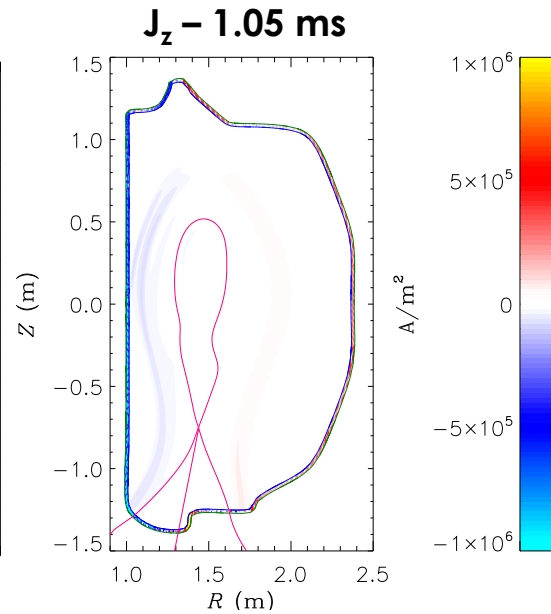
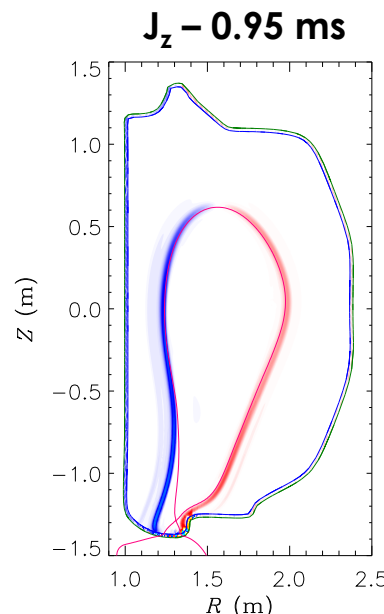
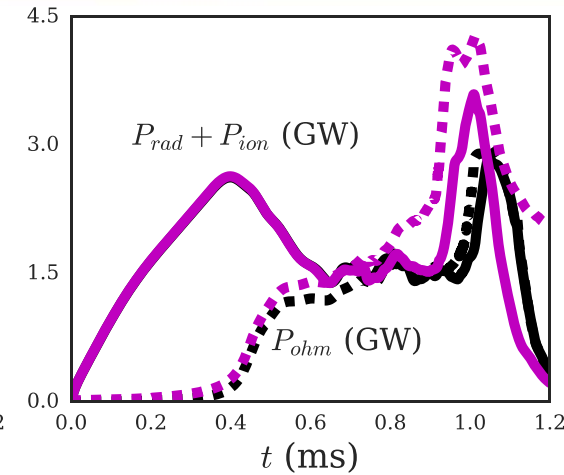
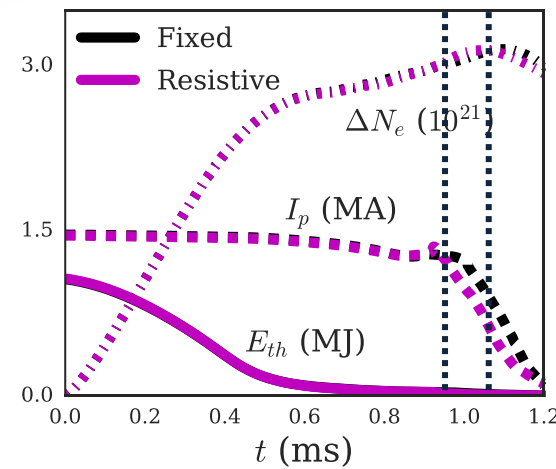
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- Results quantitatively match until contact with wall is made
- Current sheet opens and makes circuit with wall, before decaying away



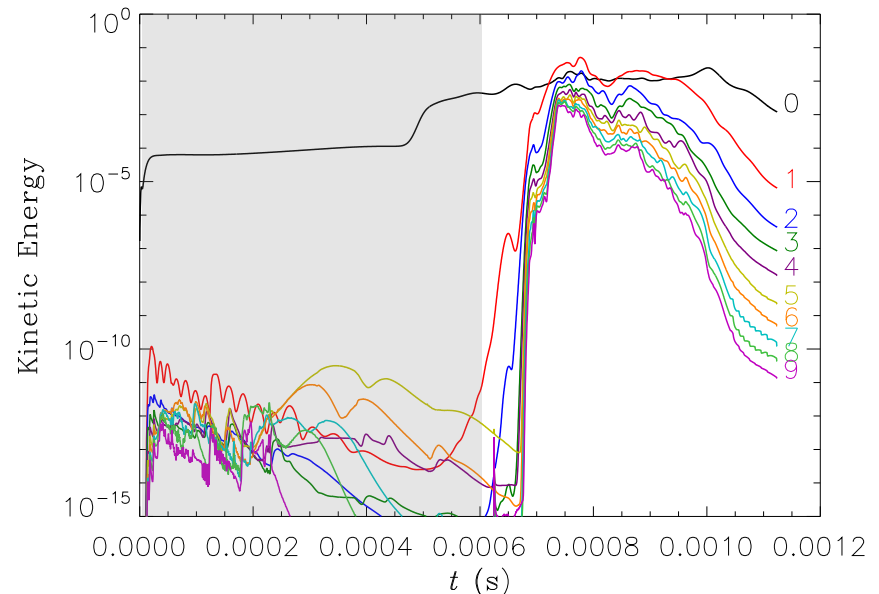
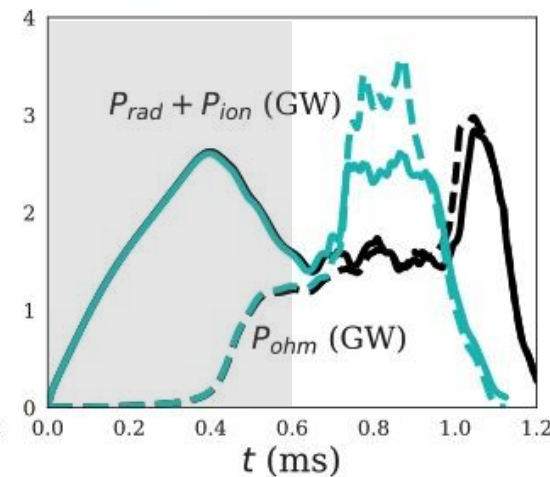
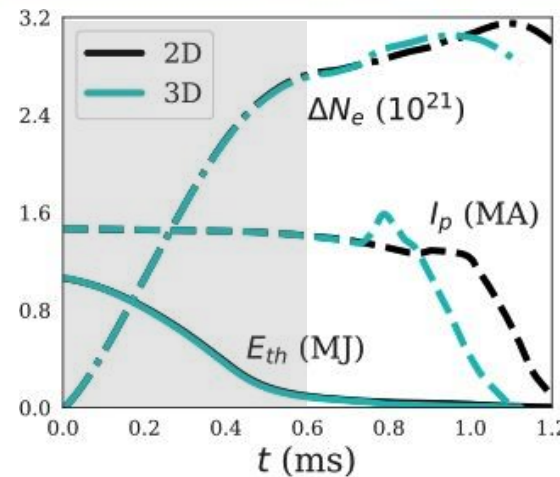
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3D M3D-C1 Modeling Shows Stable Thermal Quench, Instability-Induced Current Quench with I_p Spike

- **3D, nonlinear simulation performed with M3D-C1 using argon benchmark initial conditions**
 - 3D run is linearly stable throughout thermal quench due to axisymmetric deposition
 - Plasma sheet goes unstable, quenching current
- **Instabilities cause current to spike**
 - Axisymmetric current broadens significantly
 - First spike of this magnitude in 3D MHD simulation



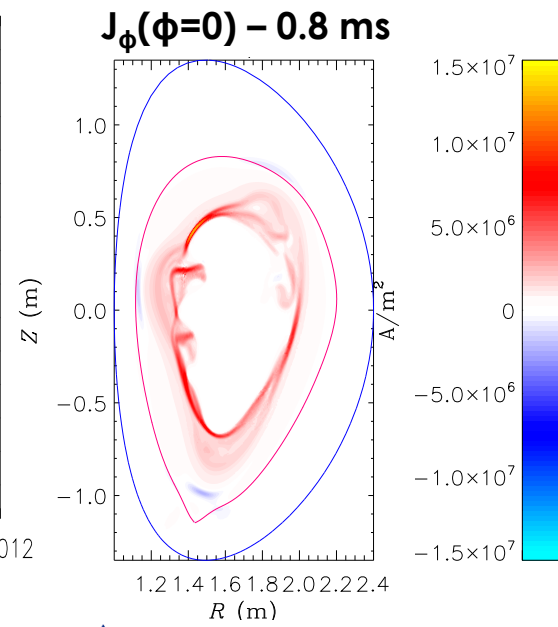
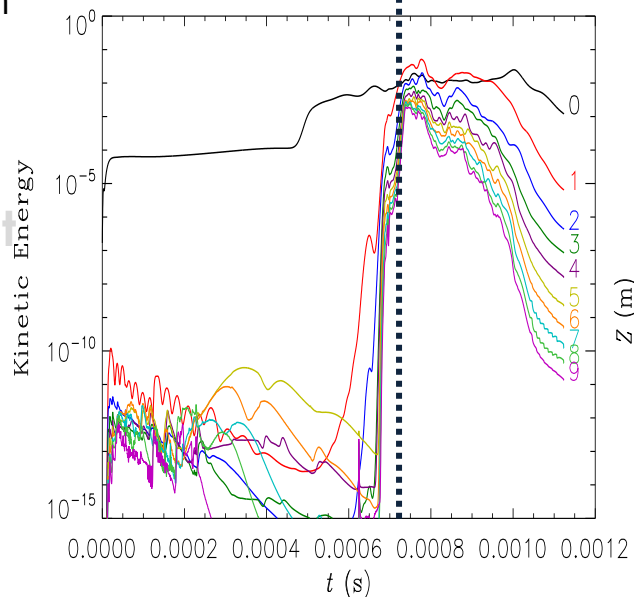
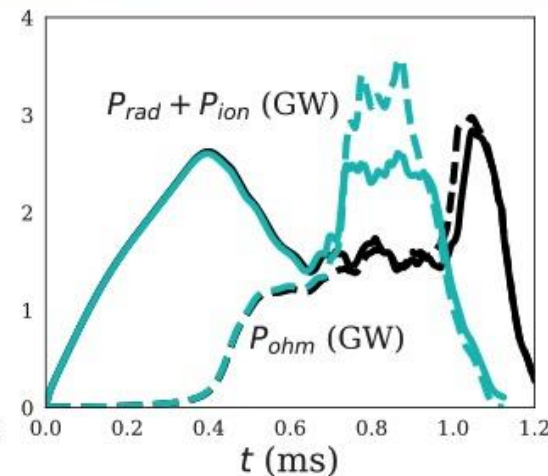
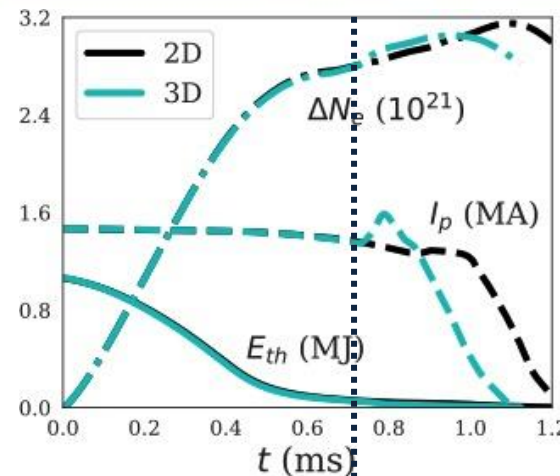
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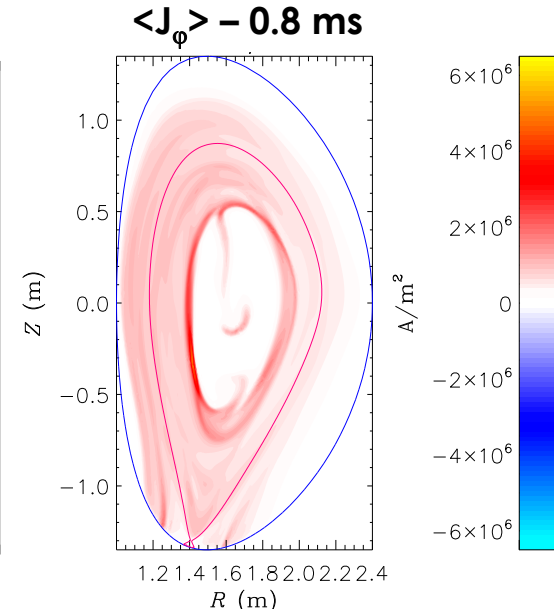
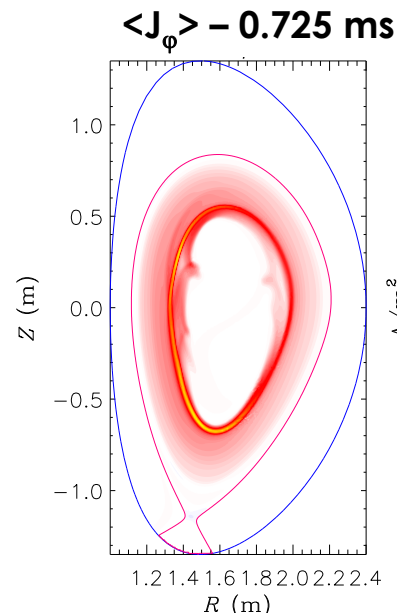
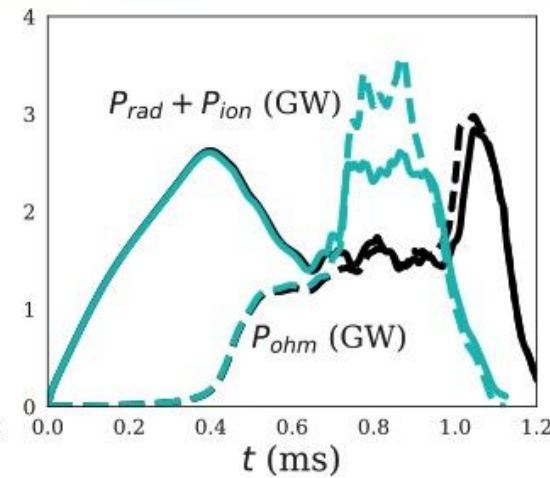
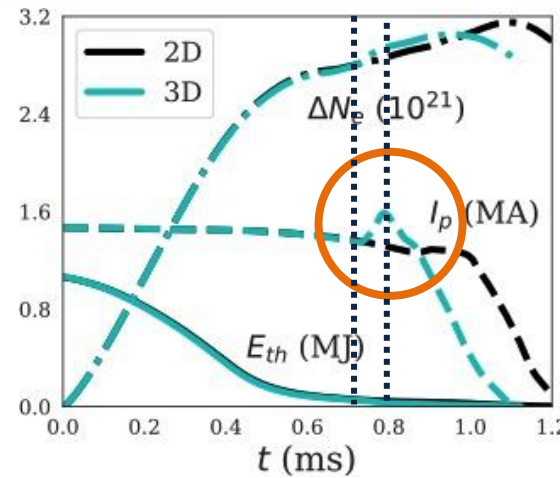
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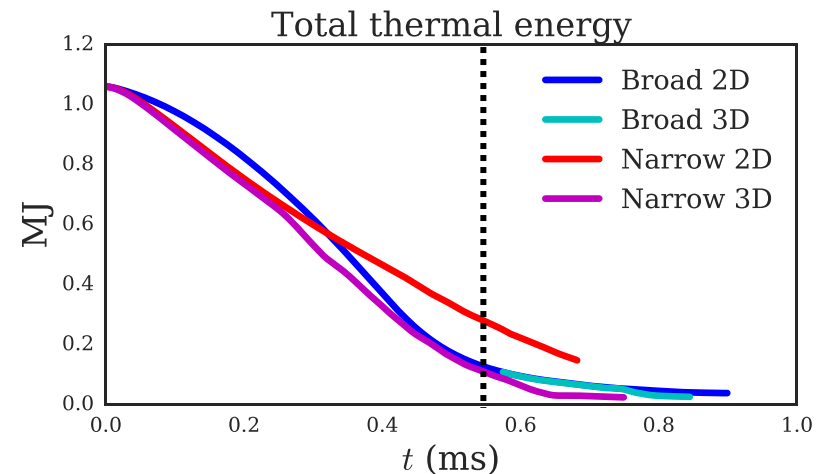
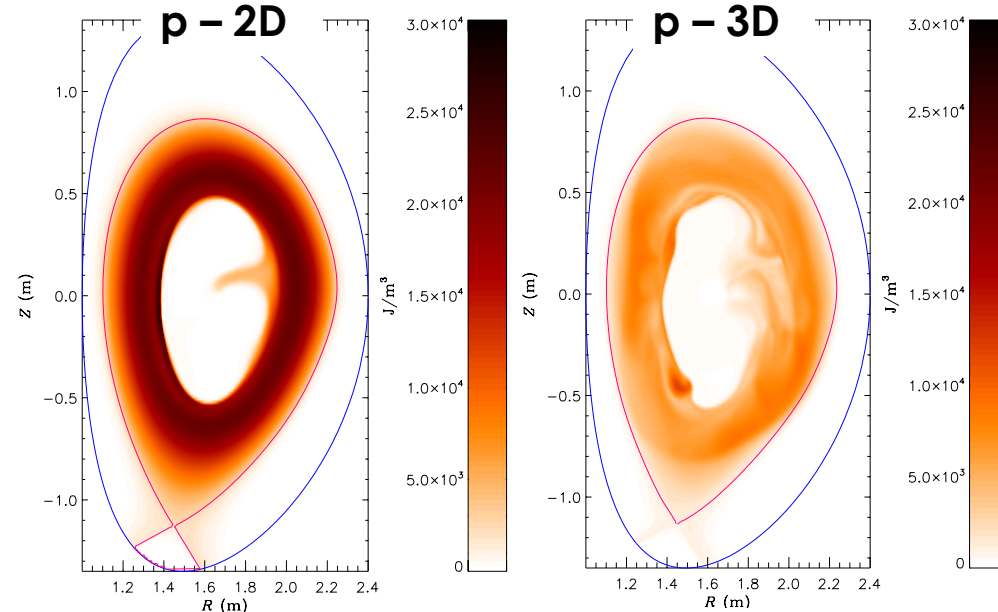
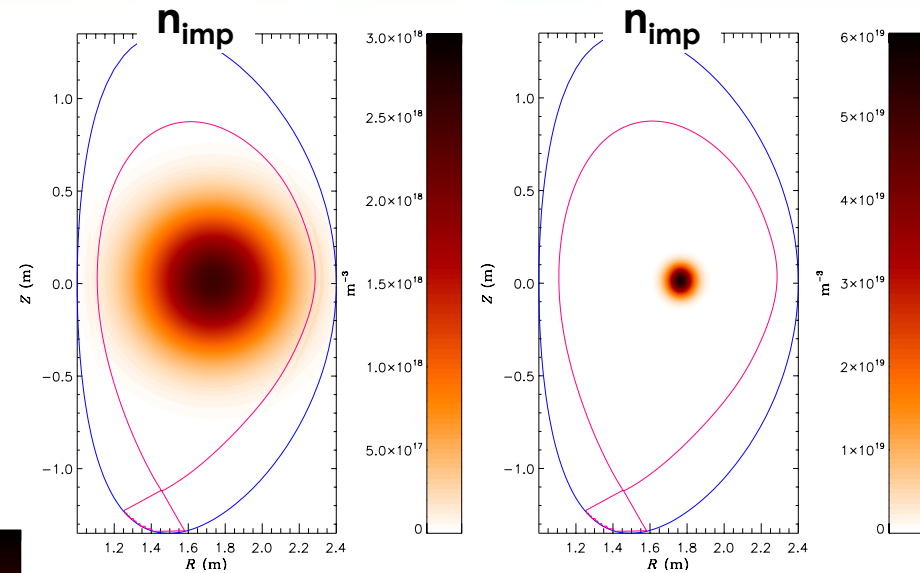
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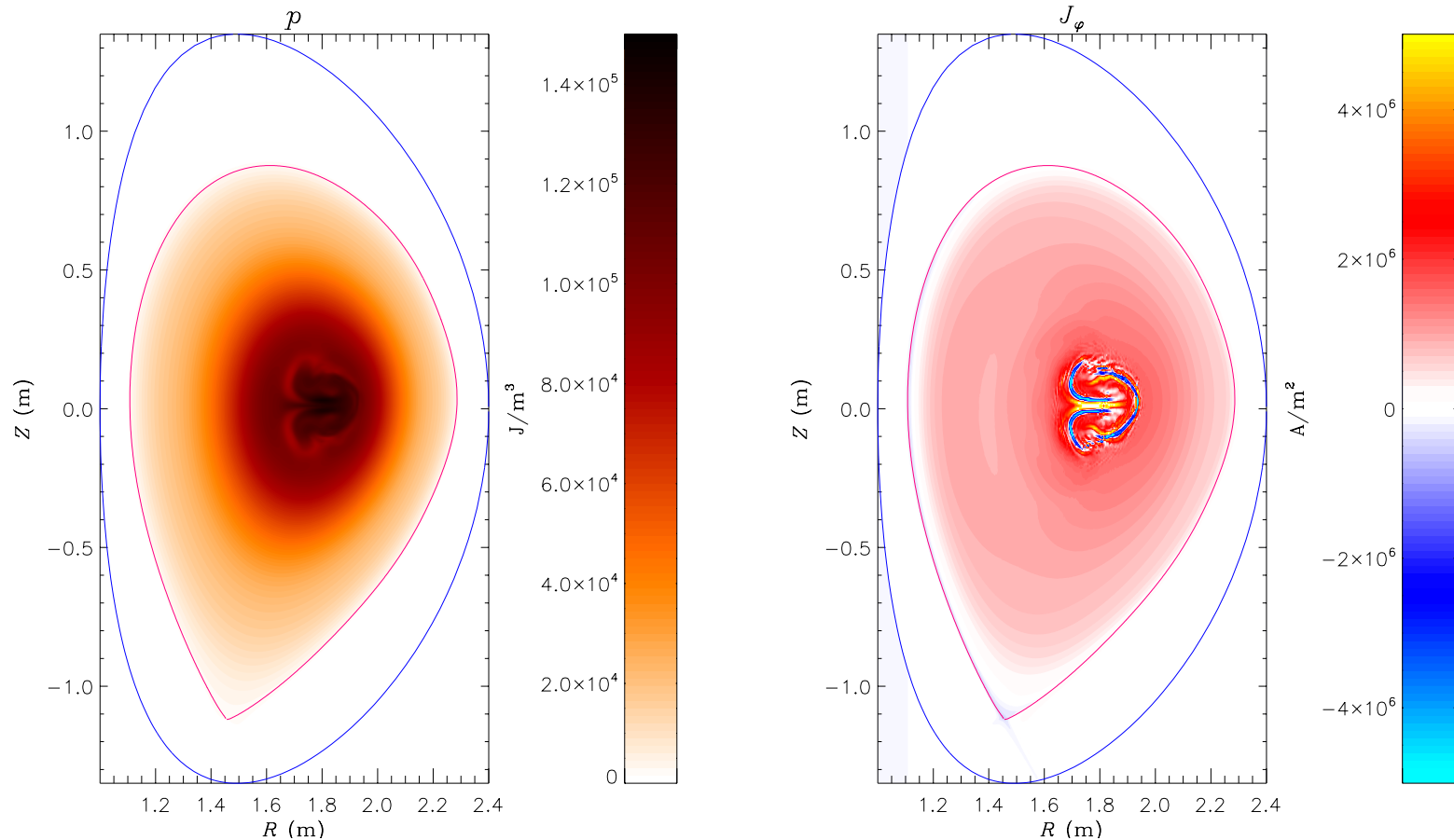
Radial Localization Demonstrates 3D Mixing

- Same total number of particles injected in broad/narrow profile
- 2D: narrow has slower thermal quench
- 3D: mixing speeds up narrow-deposition thermal quench



Toroidally Localized Deposition Causes Early, Localized Instabilities

- Physical instabilities but eventually result in numerical crash
- Requires increasing resolution or diffusivities



Ongoing/Future M3D-C1 Work

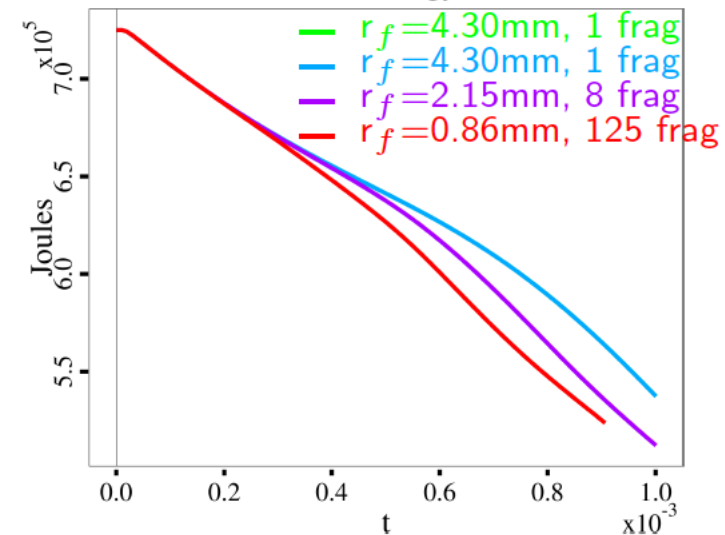
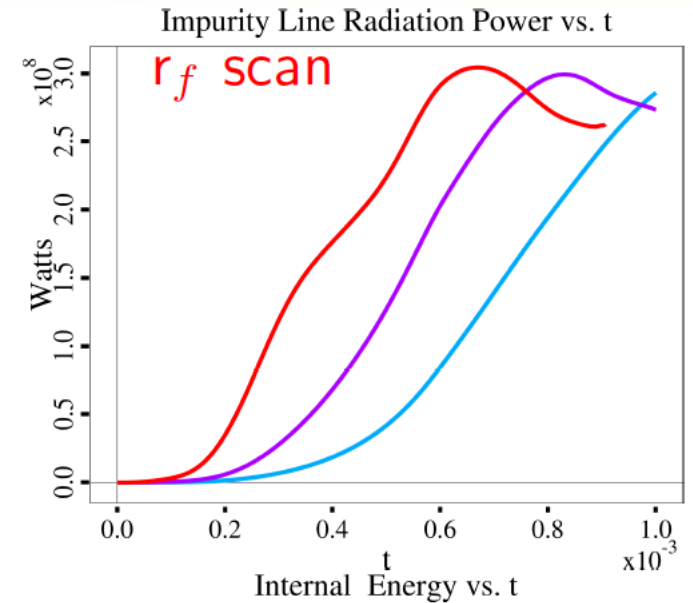
- **Complete 3D benchmark with NIMROD in near-term**
- **M3D-C1 pellet model extended allowing for multiple sources**
 - SPI fragments
 - Multiple toroidal injection
- **Focusing on simulations of toroidal localization of impurities**
 - Eventually utilize toroidal-packing capability
 - Explore impact of extended deposition in toroidal angle
 - Allow for multiple toroidal injections (high-priority for ITER)
- **Couple to Lagrangian-particle pellet-ablation code**
- **Validate simulations against experiments**
 - DIII-D in near-term
 - KSTAR and JET in later years
- **Predictive modeling for ITER**

Pellet Ablation Studies in NIMROD

C.C. Kim, J. McClenaghan

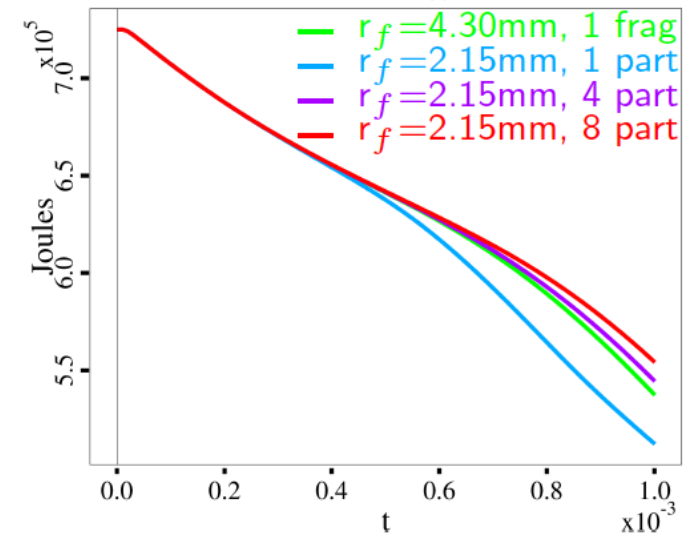
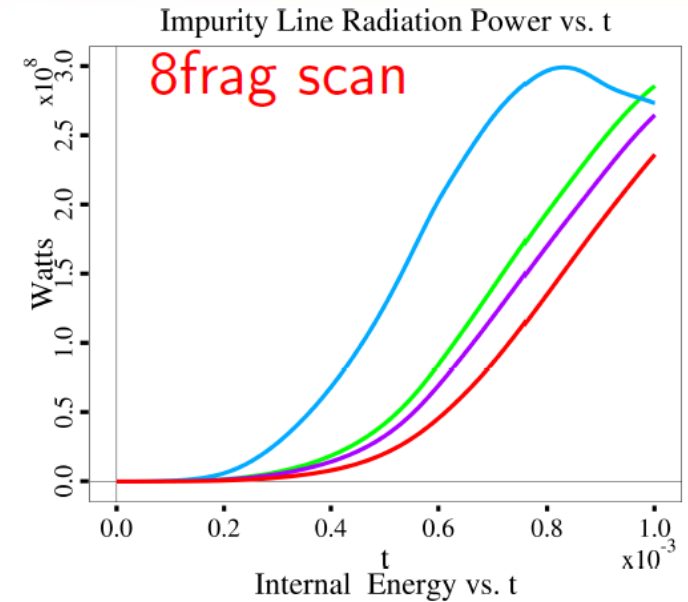
NIMROD Simulations Show Single, Monolithic May be an Adequate Approximation - Kim

- **Many small fragments increases ablation rate compared to monolithic pellet in same space**
- Increased spreading of fragments over 1 ms plume decreases ablation (purple to red)
- Increasing plume length reduces ablation (blue to purple to red)
- Increasing isotropic viscosity above 10^3 m²/s effects results
 - Despite no early MHD
 - Possibly decreases spreading, increasing shielding
- Details all result in minor variation in thermal quench time
 - $\delta\tau^{TQ} \sim 0.1$ ms
 - Plume detail cause time offset but not diverging behavior



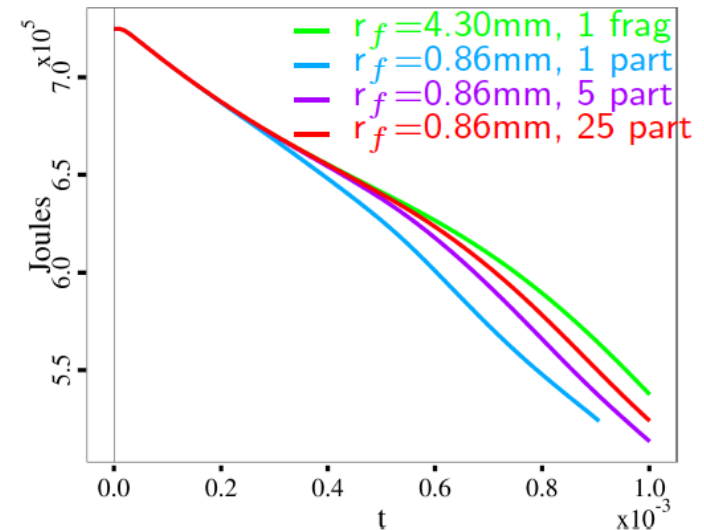
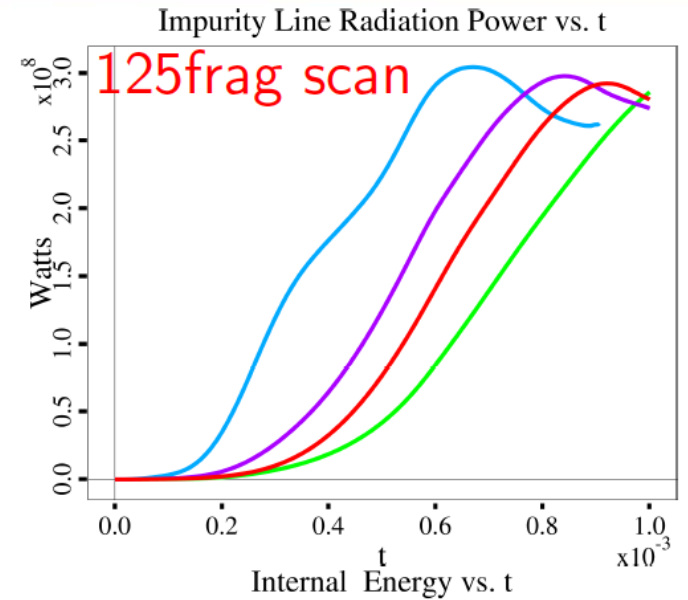
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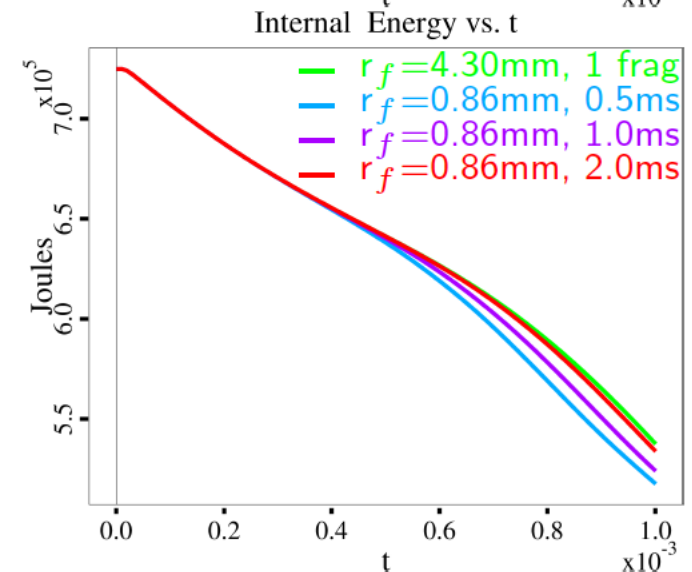
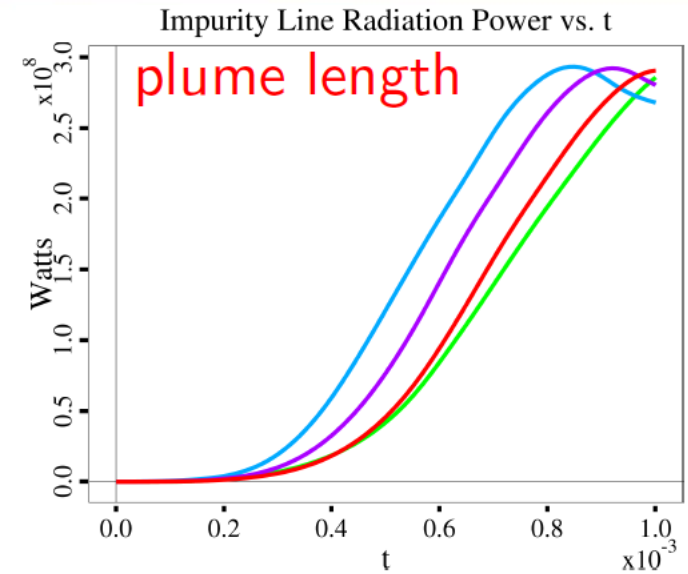
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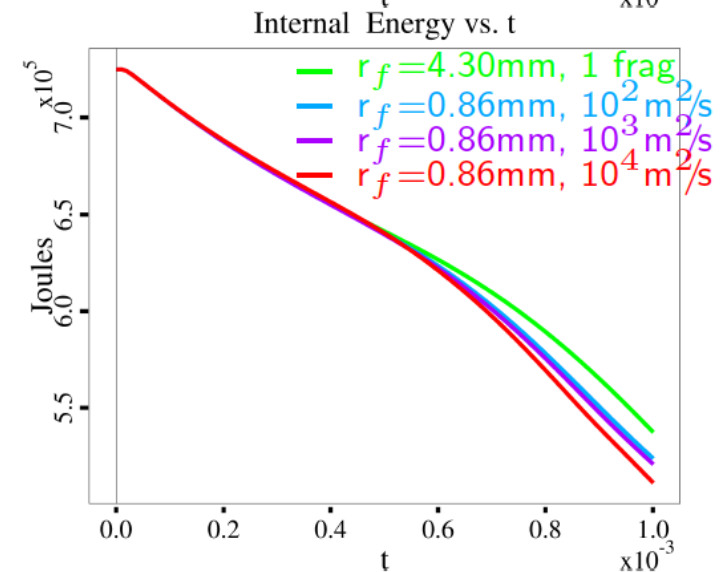
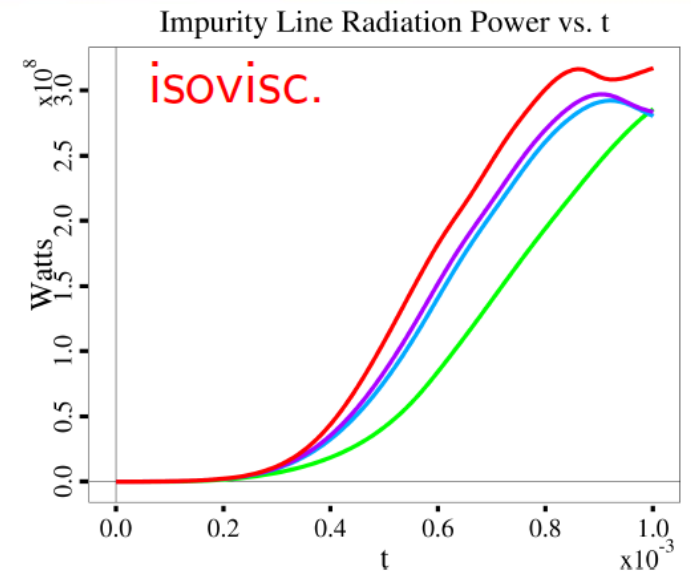
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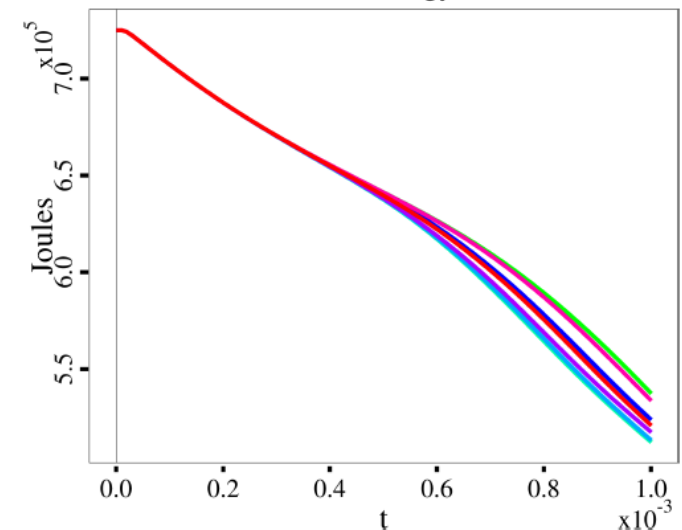
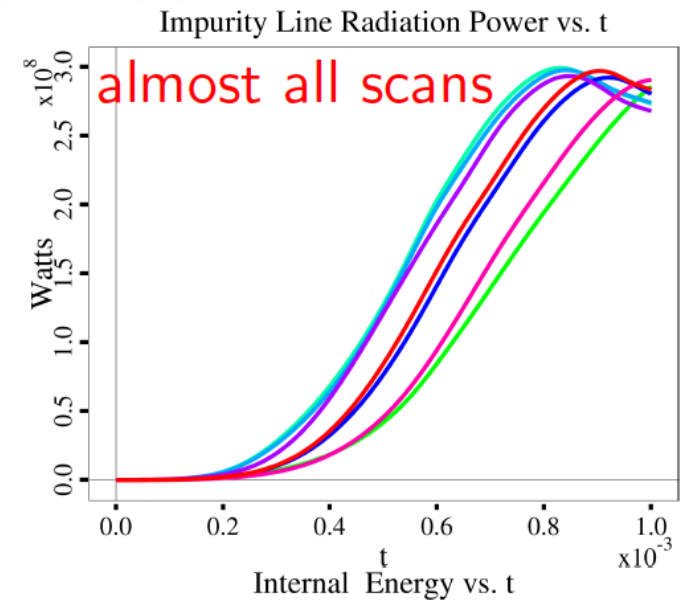
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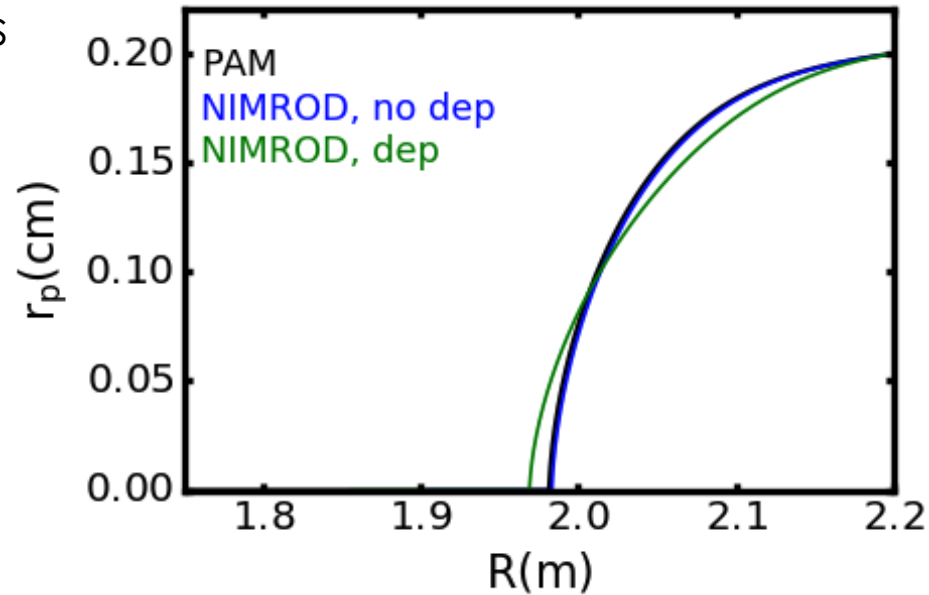


NIMROD SPI Simulations are Progressing - Kim

- **Resistivity matched to experiment:**
 $\eta = 270.0 \text{ m}^2/\text{s}$ (@ 1eV), $\eta_{\min} = 0.1 \text{ m}^2/\text{s}$ ($\approx 200 \text{ eV}$)
- **Simulations terminating due to high-n edge modes (RBM?)**
 - High viscosity not sufficient
 - Tried Chodura resistivity but not sufficient
 - Hyper-resistivity reduces iterations but still crashes
 - Trying 3D thermal conduction
 - Okay for constant κ
- **Can limit edge mode growth rate by using lower $\eta_{\max} = 10 \text{ m}^2/\text{s}$ ($\approx 10\text{eV}$)**
 - Limits Ohmic heating too much?
 - Enough for RE acceleration and current quench?
 - Maybe good enough (*10eV is pretty cold for a thermonuclear plasma*)
 - Could go unstable later, maybe a particular solution for particular equilibrium
- **High-n modes triggered by core tearing mode (2,1) and/or (3,2) ?**
 - reduce core resistivity (lower η_{\min}) to reduce trigger ?

NIMROD Pellet Ablation Implementation Verified with PAM Code - McClenaghan

- **Pellet ablation module (PAM) calculates pellet fueling deposition for transport studies**
 - Fixed n_e and T_e
 - Calculates the same equations as NIMROD
- **Benchmark setup**
 - Pure deuterium pellet
 - Outboard-midplane launch
 - $r_p = 0.2$ cm, $v_p = 500$ m/s
- **Good agreement between PAM and NIMROD when pellet is not deposited into the plasma**
- **Ablation changes when pellet is deposited into plasma**
 - Currently under investigation



Steady-State Ablation and FrontTier

P.B. Parks

Frontier Model does not Permit Steady-State Ablation

- **Frontier assumes a constant magnetic field and open (vacuum) boundary conditions in cylindrical system**
- **Lack of diamagnetism and background pressure, along with density-dependent diffusivity, result in constantly evolving radial ablation cloud**
- **Density-dependent diffusivity also requires infinitely opaque cloud in steady-state**
- **Reduced model captures these effects**
- **Steady-state would require finite background pressure, together with diamagnetic and magnetic tension forces**

Mass Density in Ablation Channel is Determined by a Convection-Diffusion Equation

- **Mass transport:**
$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_z}{\partial z} + \frac{1}{r} \frac{\partial}{\partial r} (r \rho u_r) = 0$$

- **In low- β , far-field region (away from pellet)**

- Force-balance with deeply subsonic radial flows

$$\frac{\partial p}{\partial r} = J_\theta B$$

- Ohm's Law

$$\eta_\perp J_\theta = -u_r B$$

- **Mass advects along and diffuses across field lines**

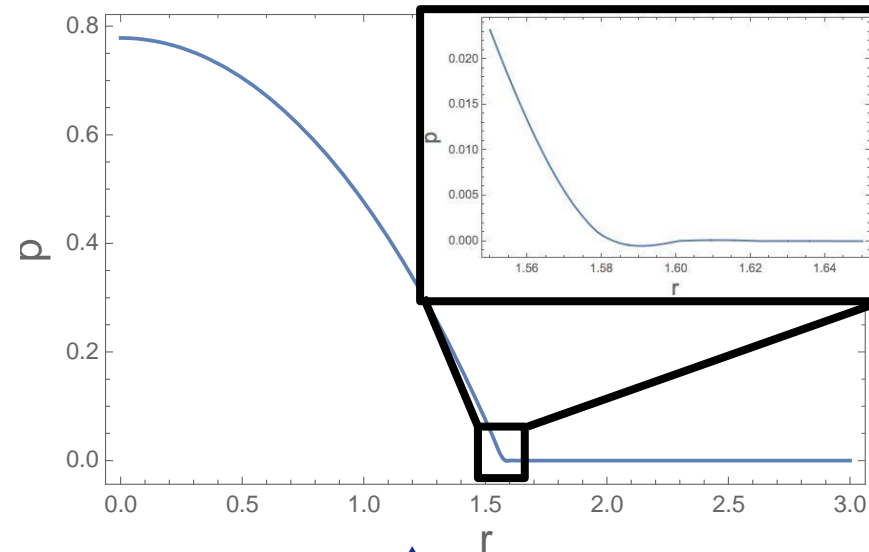
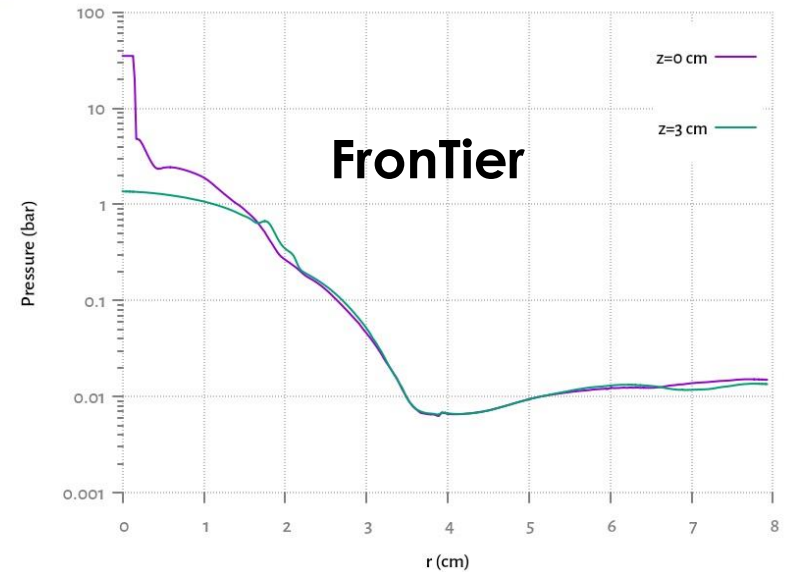
$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_z}{\partial z} = \frac{1}{B^2 r} \frac{\partial}{\partial r} \left(r \eta_\perp \rho \frac{\partial p}{\partial r} \right)$$

- **or, if T is constant,**
$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_z}{\partial z} = \frac{1}{r} \frac{\partial}{\partial r} \left(r \mathbf{D}_\perp \frac{\partial \rho}{\partial r} \right)$$

$$\mathbf{D}_\perp = \frac{\eta_\perp p}{B^2}$$

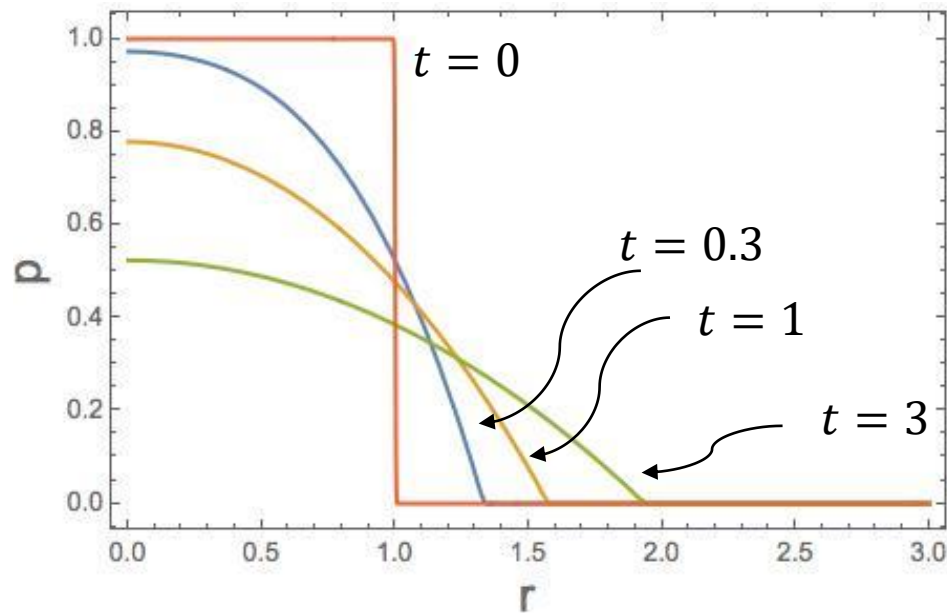
Finite Pressure Gradient Continuously Expands into Vacuum Region – No Steady-State

- **Pressure profiles in FrontTier and reduced model have similar global structure**
- Boundary of channel moves deeper into vacuum region
- **Steady-state would require**
 - Finite background pressure to raise diffusion
 - Diamagnetic currents to support pressure step at boundary



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Model Also Results in Infinite Opacity

- **Finite opacity required or no heat flux to pellet (no ablation)**

- $\tau_{axis} = \int_{z_s}^{\infty} \rho dz \neq \infty$
- Density ρ must fall off faster than $1/z$ for large z

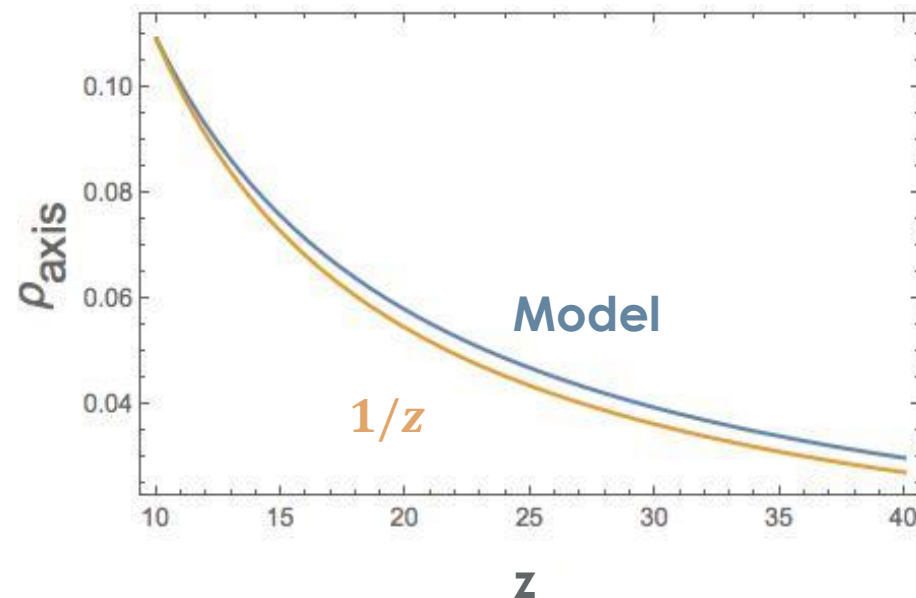
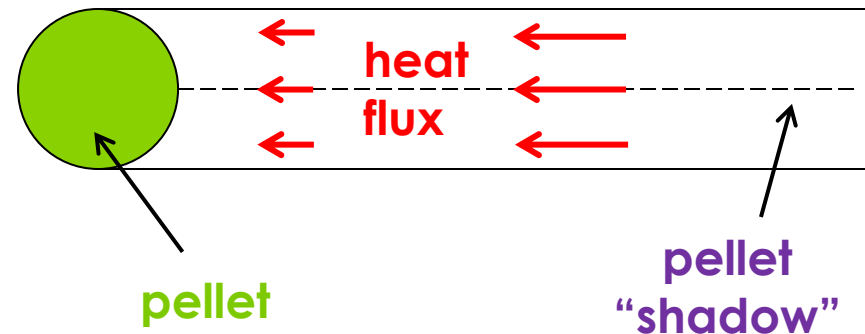
- **Reduced model gives logarithmic divergence in opacity**

- True even with u_z linearly increasing with z
- More optimistic assumption than sublinear profile found in Frontier

- **Not enough diffusion in far-field to allow for finite opacity**

- **Requires other means to make finite-length ablation cloud**

- Moving pellet
- Curvature drift



Acknowledgments

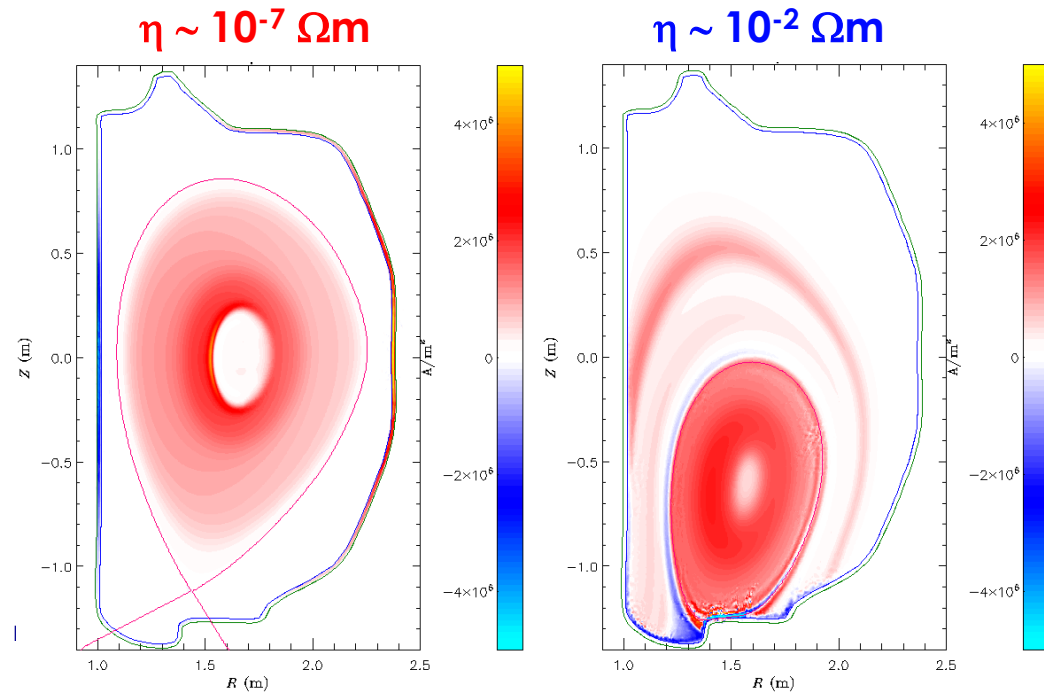
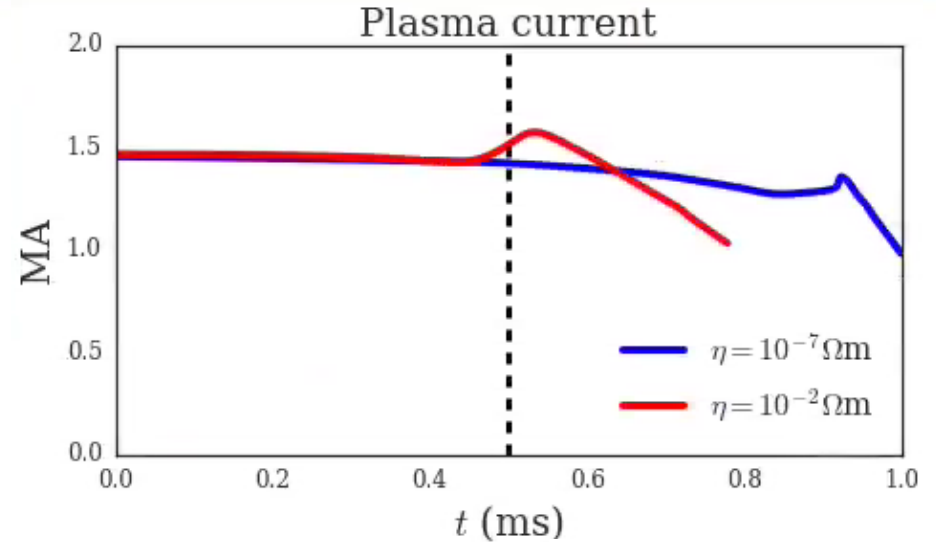
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 - DE-FG02-95ER54309,
 - DE-FC02-04ER54698,
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Additional Slides

Higher resistivity allows must faster vertical displacement

- **Future work**

- Optimal mesh to resolve wall contact
- Match experimental L/R wall time



Summary

- Frontier is a time-dependent simulation of pellet ablation in a stationary B field surrounded by vacuo (**Open Boundary Conditions**)
- We developed a reduced model that shows **no steady state** is possible when a magnetized **resistive medium** (pellet cloud) expands into a **vacuum**
- We proved that stationary radial confinement of cloud is only possible when our **resistive medium** is surrounded by an **ideal medium** (hot plasma). Cloud is radially confined by **diamagnetic surface current layer**
- Our Convection diffusion model proved that in steady state the opacity of the cloud along the **pellet shadow** has a logarithmic divergence which prevents steady ablation rate. Cloud length must be limited? How?
 - 3D effects necessary, e.g., pellet motion and Alfvén wave damping, curvature drift drive (Parks 1992, 2000, 2005, Rozhansky 1994)

Reduced Model leads to Axisymmetric Convective Diffusion Equation

- **Axisymmetric Steady-State Momentum Transport**

- **z component** $\rho \left(u_z \frac{\partial u_z}{\partial z} + u_r \frac{\partial u_z}{\partial r} \right) = - \frac{\partial p}{\partial z}$

- **r component** $\rho \left(u_r \frac{\partial u_r}{\partial r} + u_z \frac{\partial u_r}{\partial z} \right) = - \frac{\partial p}{\partial r} + J_\theta B$

- **Mass Transport** $\frac{\partial \rho}{\partial t} + \frac{\partial \Gamma_{\parallel}}{\partial z} = - \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \Gamma_{\perp}}{\partial r} \right)$ $\Gamma_{\parallel} = \rho u_z$
 $\Gamma_{\perp} = \rho u_r$

- **In low- β far-field region the strong magnetic field inhibits radial flow**


- Ignore inertial terms in radial component of momentum equation

$$\rho \left(u_r \frac{\partial u_r}{\partial r} + u_z \frac{\partial u_r}{\partial z} \right) = - \frac{\partial p}{\partial r} + J_\theta B$$

The equation above is crossed out with a large red 'X' and red arrows pointing to the inertial terms $u_r \frac{\partial u_r}{\partial r}$ and $u_z \frac{\partial u_r}{\partial z}$, indicating they are to be ignored.

In the Far-Field region of the Cloud the Radial flow Velocity is Diffusive like

- **Cross-field Force balance** $\frac{\partial p}{\partial r} = J_{\theta} B$
- **Ohm's law** $\eta_{\perp} J_{\theta} = -u_r B$
- **Eliminate current density J_{θ} to get radial flow**

 $u_r = -\frac{\eta_{\perp}}{B^2} \frac{\partial p}{\partial r}$

Mass Density in Ablation Channel is determined by a **Convection-Diffusion** Equation

$$\rightarrow \frac{\partial \rho}{\partial t} + \frac{\partial \rho u_z}{\partial z} = \frac{1}{B^2 r} \frac{\partial}{\partial r} \left(r \eta_{\perp} \rho \frac{\partial p}{\partial r} \right) \quad p = \frac{\rho}{m} (1 + Z) T \quad \eta_{\perp} = \frac{m_e v_{ei}}{n_e e^2} = \frac{Z \ln \Lambda_{ei}}{9700 T (\text{eV})^{3/2}}$$

(pressure) (Spitzer cross-field electrical resistivity)

– Expanding out

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_z}{\partial z} = \frac{1}{m B^2 r} \frac{\partial}{\partial r} \left\{ r \eta_{\perp} \rho \left[\underbrace{(1 + Z) T \frac{\partial \rho}{\partial r}}_{- \text{ (large) }} + \underbrace{(1 + Z) \rho T \frac{\partial T}{\partial r}}_{+ \text{ (small) }} + \underbrace{\rho T \frac{\partial Z}{\partial r}}_{+ \text{ (small) }} \right] \right\}$$

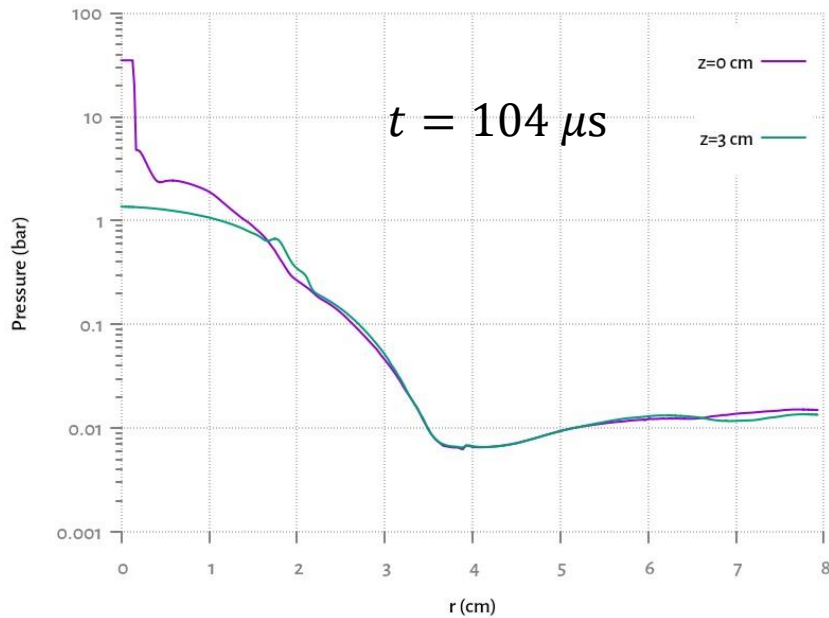
- Keeping large term only:

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_z}{\partial z} = \frac{1}{r} \frac{\partial}{\partial r} \left(r \mathbf{D}_{\perp} \frac{\partial \rho}{\partial r} \right) \quad \mathbf{D}_{\perp} = \frac{\eta_{\perp} p}{B^2} \quad \leftarrow \text{classical cross-field diffusion coefficient for fully ionized plasma}$$

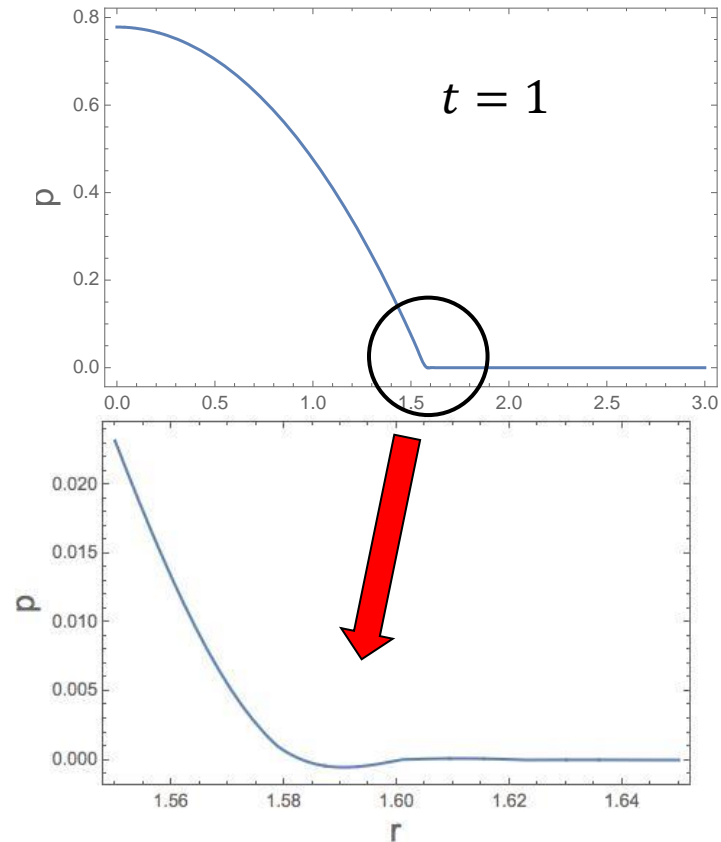
- Get same classical diffusion coefficient from the microscopic picture

$$D_{\perp} \sim \frac{(\text{electron gyro radius})^2}{\text{electron - ion collision time}}$$

Frontier Radial Pressure profiles has similar global structure as Parks' Reduced Model



— Frontier Simulation

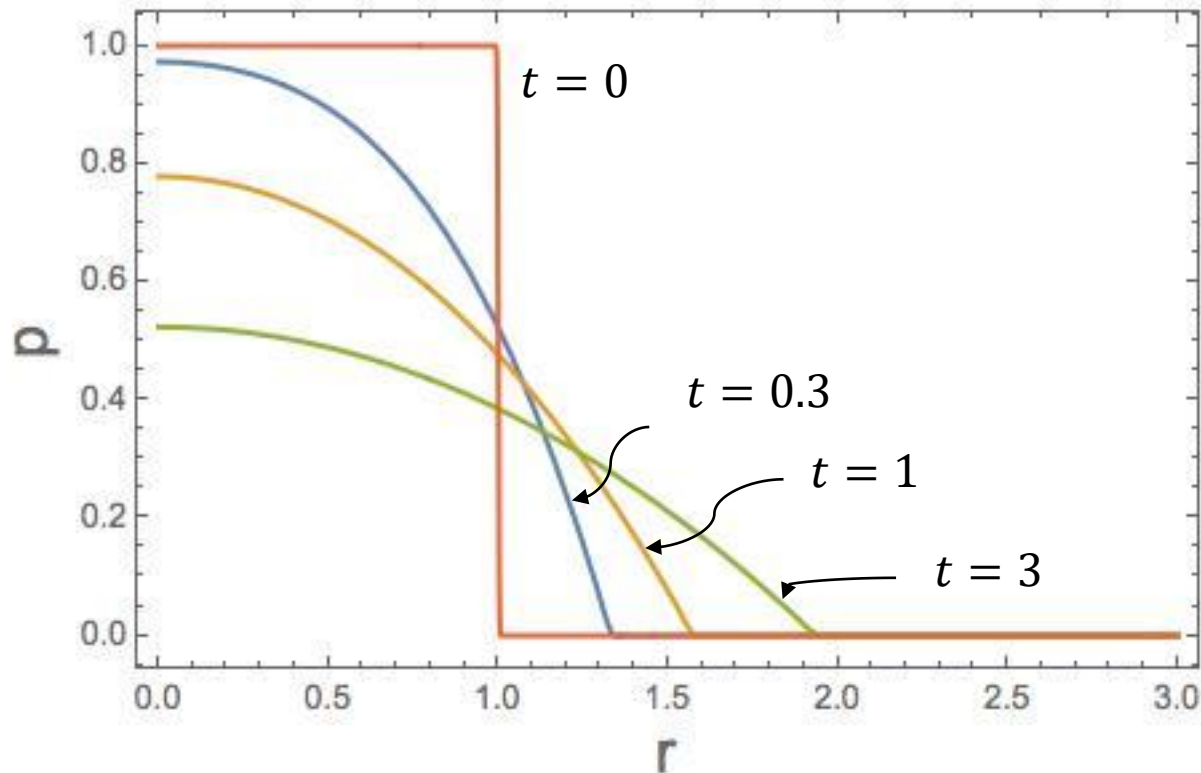


— Reduced model

- Radial flow velocity is zero when $dp/dr = 0$. But $dp/dr = 0$ when $p \sim 0$. in Frontier and in Parks model. That's a physical inconsistency!
Cloud keeps expanding to find a new point where $dp/dr = 0$

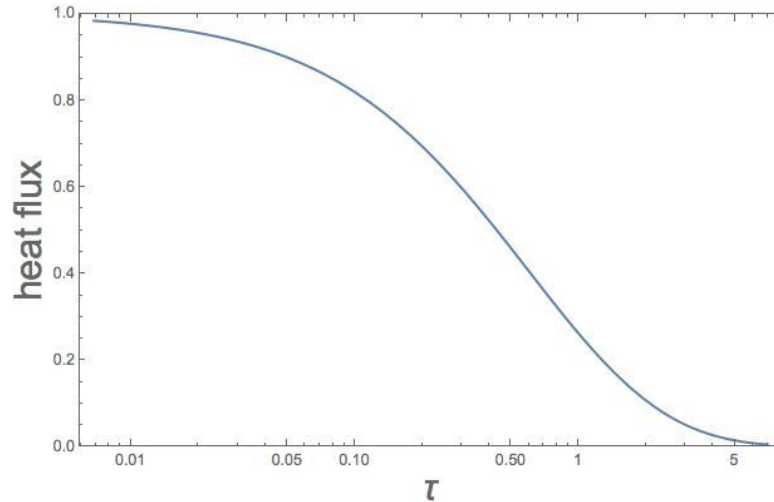
No steady state is possible with open (vacuum) Boundary conditions

- Radial profiles at various times shows that the $vr \propto dp/dr = 0$ point keeps moving deeper and deeper into the vacuum region (no steady state)



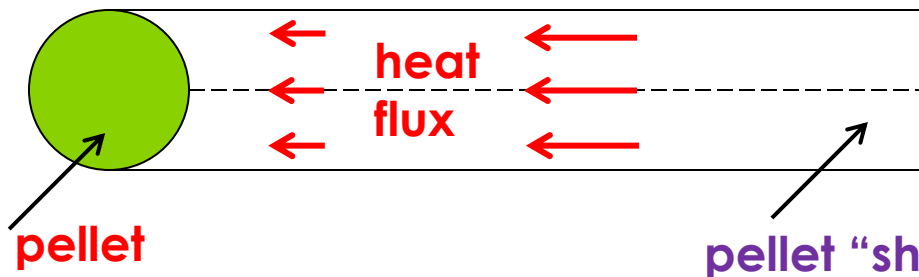
Steady-State also Demands Finite Opacity along Pellet Shadow

- Attenuation of kinetic electron heat flux with increasing **opacity**



$$\tau(z) = \int_z^{\infty} \rho(r, z) dz$$

- The cloud “opacity” on axis **must not diverge**, otherwise the fast electrons would never reach the pellet and it would cease to ablate



$$\tau_{axis} = \int_{z_s}^{\infty} \rho dz \neq \infty$$

Equivalent to saying that the density ρ must fall off faster than $1/z$ for large z

Assume parallel flow velocity increases linearly with axial distance

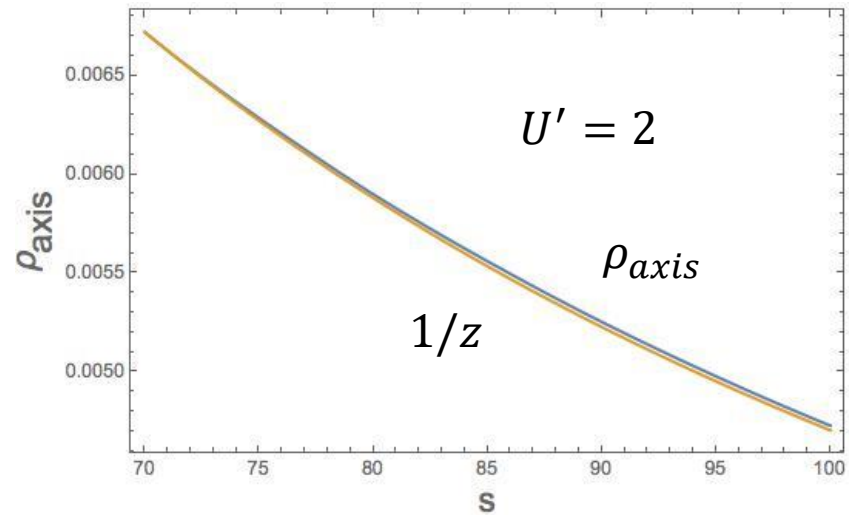
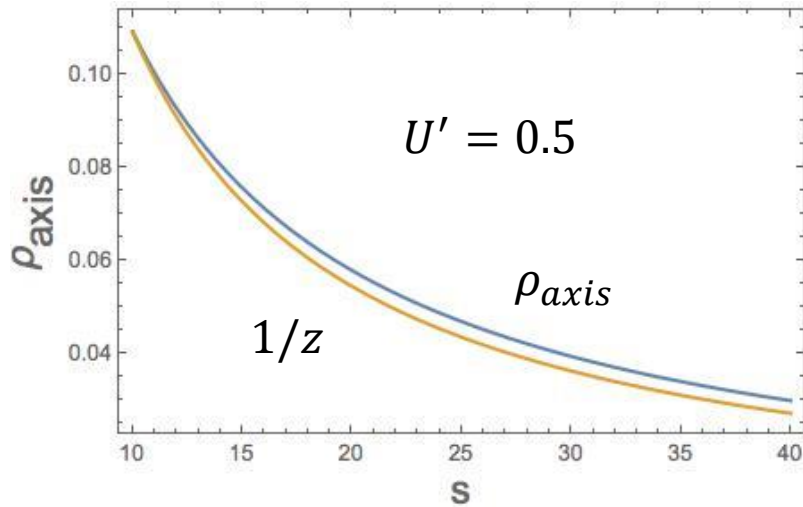
$$U(z) \equiv \frac{u_z}{u_{z0}} = 1 + U' \cdot z$$

$U' = \text{const velocity gradient}$

- **New Non-Linear equation in steady state becomes**

$$(1 + U' \cdot z) \frac{\partial \tilde{\rho}}{\partial z} = -\tilde{\rho} U' + \frac{1}{4r} \frac{\partial}{\partial r} \left(r \tilde{\rho} \frac{\partial \tilde{\rho}}{\partial r} \right)$$

The $\tilde{\rho}_{axis}$ tends to fall off faster with a linearly increasing parallel velocity



- Opacity diverges logarithmically since the axial density profile falls off slower than $1/z$

$$\tau_{axis} = \int_{z_s}^{\infty} \rho dz \quad \text{---} \rightarrow \quad \infty$$