

# C – pellet disruption mitigation modeling with M3D-C1

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CTTS Talk Series





# C – pellet disruption mitigation modeling with M3D-C1

## Outline:

- Motivation
- C ablation model
- Validation/comparison (ASDEX-U)
- Modelling pellets in M3D-C1
- NSTX simulations
  - Convergence study
- Summary and future work



# C – pellet disruption mitigation modeling with M3D-C1

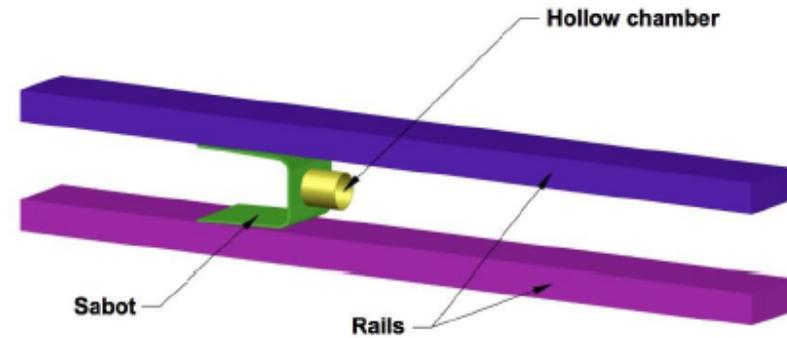
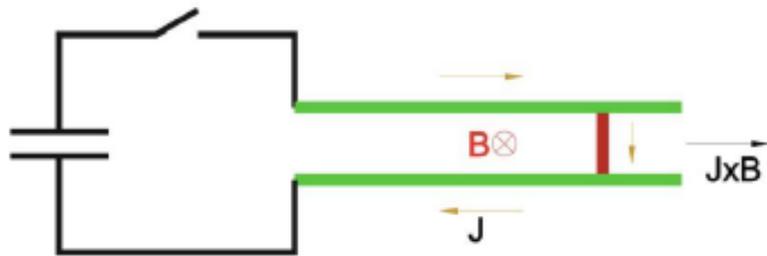
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# Motivation

- An Electromagnetic Pellet Injector (EPI) has been developed \*
- EPI would offer advantages for ITER
  - Very fast response time (2-3 ms)
  - Speeds up to 1 km/s
- Proposal to test on NSTX-U.



- We have started single C-pellets injection simulations using M3D-C1
  - C-ablation model has been incorporated.
  - Simulations on NSTX-U are being conducted:
    - Convergence study
    - TQ quench sensitivity on modelling parameters
    - Understanding the physics involved



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# C ablation model

- Sergeev et al., Plasma Phys. Rep. 32 (2006) 363
- Sergeev et al., ECA 18B (1994) 1364
- Kuteev et al., Sov. J. Plasma Phys. 10 (1984) 675

## Based on a Neutral Gas Shielding Model (NGS)

- Key quantity is  $\delta = q_p/q_0 \rightarrow$  shielding factor
  - $q_p \rightarrow$  heat flux reaching the pellet surface
  - $q_0 \rightarrow$  heat flux from the surrounding plasma
- Hydrogen pellets (strong shielding)
  - Low sublimation energy  $\varepsilon$
  - $\delta \ll 1$ : Most of the plasma heat flux is absorbed by the neutral pellet cloud
- Refractory pellets (weak shielding)
  - High sublimation energy
  - $\delta \geq 0.8$ : Most of the plasma heat flux reaches the pellet surface
  - Delayed time at which evaporation begins



# C ablation model

For both limits ( $\delta \rightarrow 0$  and  $\delta \rightarrow 1$ ) analytical expressions for the ablation rate  $\dot{N}$  is derived

## Strong shielding ( $\delta \rightarrow 0$ )

Based on scaling laws

$$\dot{N}_0 \left[ \frac{\text{Atom}}{\text{s}} \right] \cong 1.94 \times 10^{14} n_e^{0.45} [\text{cm}^{-3}] \times T_e^{1.72} [\text{eV}] r_p^{1.44} [\text{cm}] \varepsilon^{-0.16} [\text{eV}] \times A_p^{-0.28} [\text{amu}] Z_p^{-0.56} (\gamma - 1)^{0.28}$$

Tabulated for various materials

## Weak shielding ( $\delta \rightarrow 1$ )

$$\dot{N}_\delta \left[ \frac{\text{Atom}}{\text{s}} \right] \cong \frac{\delta}{\varepsilon} r_p^2 n_e \sqrt{\frac{8\pi T_e^3}{m_e}}$$

$$\delta^{-1} = 1 + \frac{1.725\sqrt{\pi}(\pi - 2)Z_p e^4 r_p n_e E_1(I_{eff}/T_e)}{\varepsilon V_s \sqrt{2 m_e T_e}}$$

$$V_s = \sqrt{\gamma T_s / m_p} \quad T_s \approx 5000 \text{ K}$$

Also applicable to Li, Be, B

However, C pellet can have an **intermediate shielding**

- There is no analytical model for this regime
- They propose a standard interpolation:

$$\dot{N} = \frac{\dot{N}_0 \dot{N}_1}{\dot{N}_0 + \dot{N}_1}$$

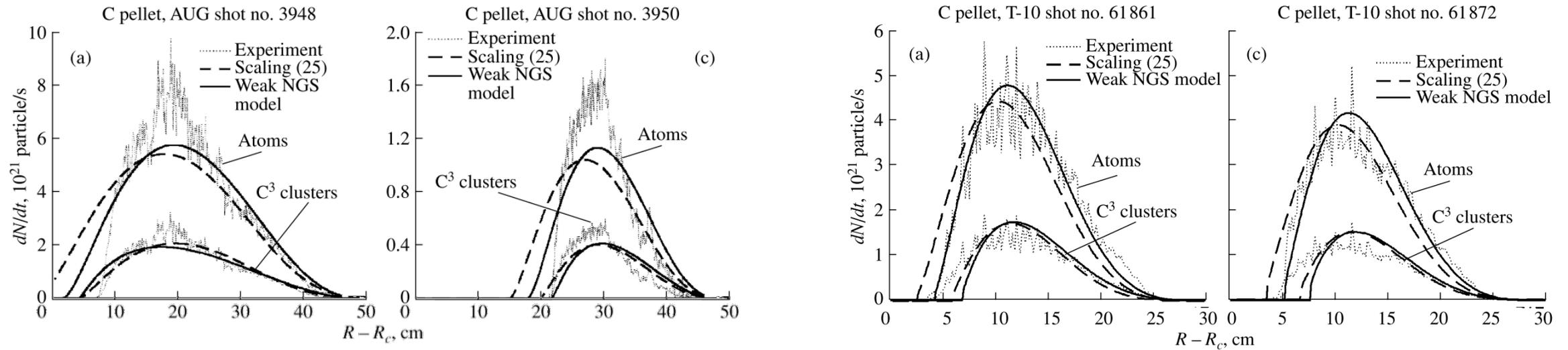
Expression we have implemented in M3D-C<sup>1</sup>



# Model were tested with experimental data

Ablation rate model was tested in several discharges obtaining good agreement

- No MHD evolution



AUG #3948

AUG #3950

T-10 #61861

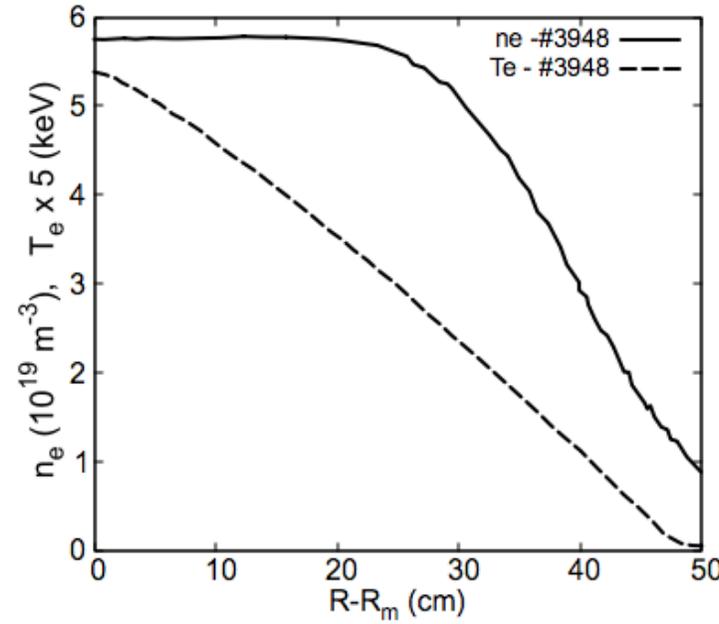
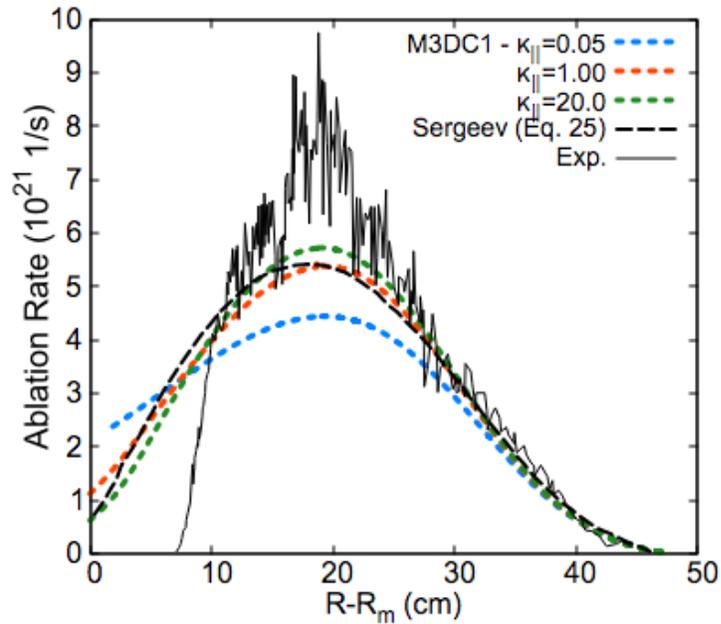
T-10 #61872

It was also tested for different pellet materials



# M3D-C1 implementation also tested

We tested our implementation in an AUG-#3948-like plasma (no G-EQDSK available)



Parameter	#3948
$r_p$	0.25 mm
$v_p$	485 m/s
$B_0$	1.96 T
$I_p$	0.8 MA
$R_0$	1.7 m
Enlong.	1.6
$\kappa_{\perp}$	$3 \cdot 10^{-6}$

Agreement is very good.

Main modeling features in M3D-C1:

- Pellet neutral cloud is prescribed
- Plasma evolves self-consistently in time



# Modelling pellets in M3D-C1

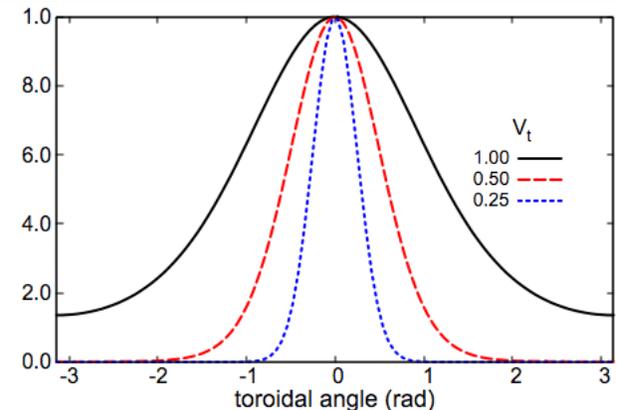
The ablated material (given by  $\dot{N}$ ) is weighted by the neutral cloud distribution  
Spatial distribution for the neutral cloud is prescribed:

$$S = \frac{1}{(2\pi)^{3/2} V_p^2 V_t} \exp \left[ -\frac{(R - R_p)^2 + (Z - Z_p)^2}{2 V_p^2} - \frac{R R_p (1 - \cos(\varphi - \varphi_p))}{V_t^2} \right]$$

- Thus, The size of the neutral cloud has to be specified ( $V_p$ ,  $V_t$ ). Limitations arise due to mesh size and number of toroidal planes.
- Smaller cloud sizes require more toroidal planes and smaller time steps.

**Example:** In NSTX-U  $R_{out} \sim 1.4$  m. Thus, the minimum toroidal neutral cloud size scales roughly as

# tor. Planes	$V_t$
8	$\approx 1.00$ m
16	$\approx 0.50$ m
32	$\approx 0.25$ m





# Modelling pellets in M3D-C1

## Plasma evolves self-consistently in time

- B. Lyons, C. Kim, Y. Liu, N. Ferraro, S. Jardin, J. McClenaghan, P. Parks, L. Lao, Plasma Phys. and Contr. Fusion **61** 064001 (2019)
- N.M. Ferraro, B. C. Lyons, C.C. Kim, Y.Q. Liu, and S.C. Jardin, Nucl. Fusion **59** 016001 (2019)
- Single fluid equations (same velocity,  $\mathbf{v}$ , for all species ( $e, i, Z^j$ ))
- Continuity equation for each ion species
  - $\frac{\partial n_i}{\partial t} + \nabla \cdot (n_i \mathbf{v}) = D \nabla^2 n_i + \sigma_i$  (same for  $n_Z^j$ )
  - Electron density is defined to satisfy quasi-neutrality
- $\sigma_Z^j$  is calculated using KPRAD module (ionization, recombination)
- All ionized impurities ( $Z^j$ ) have the same temperature as the main ion species,  $T_i$
- Two temperature equations ( $\Sigma$ ions and  $e^-$ ) also include the radiation losses calculated by KPRAD



# C – pellet disruption mitigation modeling with M3D-C1

## Outline:

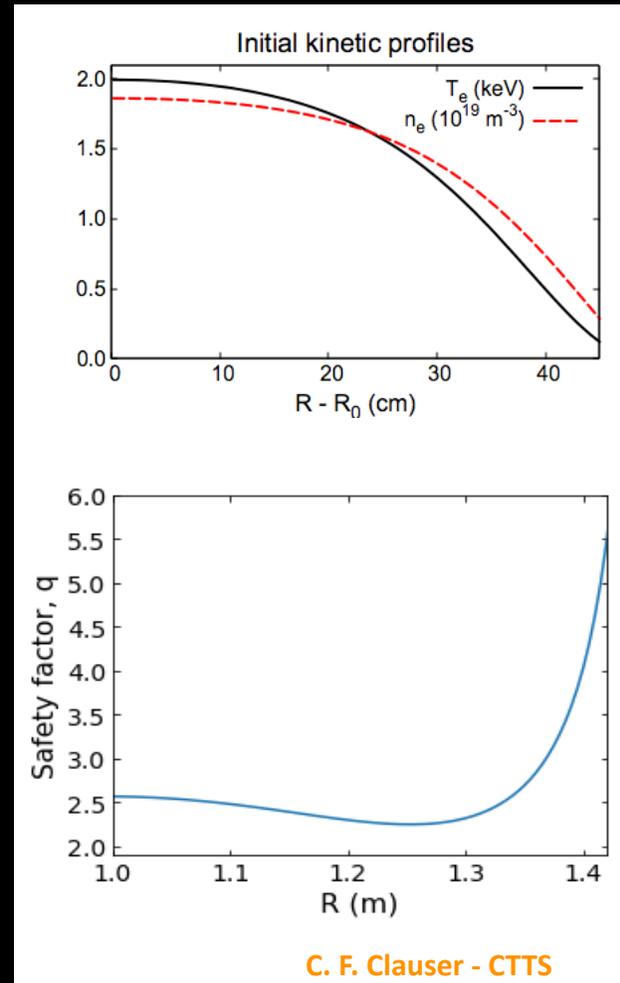
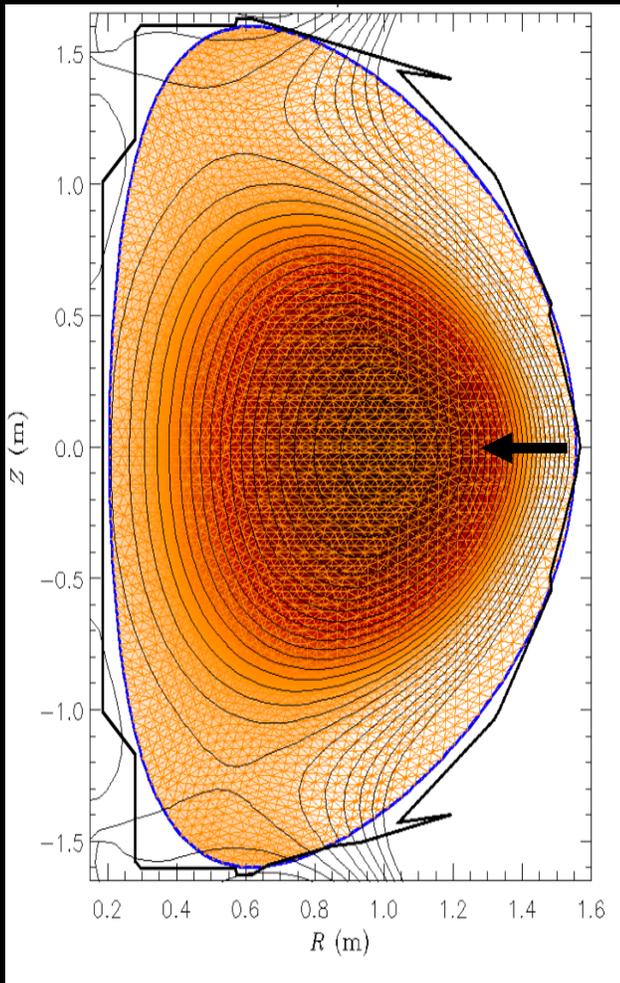
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# NSTX-U C-pellet Disruption Mitigation Study

We studied single C-pellet injection in NSTX-U (#139536) to support EPI proposal

We started from equilibrium (g-eqdsk provided) and injected a C-pellet radially at the midplane



Parameter	#139536
$T_{e0}$	2 keV
$n_{e0}$	$\sim 2 \times 10^{19} \text{ m}^{-3}$
$B_0$	0.44 T
$I_p$	0.58 MA
$R_0$	0.99 m
$\beta$	2.25 %

C. F. Clauser - CTTS



# NSTX-U C-pellet Disruption Mitigation Study

- **We carried out a scan over different parameters**
  - **Modelling & other parameters**
    - Transport and other parameters (density diffusion, viscosity)
    - Pellet neutral cloud size ( $V_p$  &  $V_t$ )
  - **Pellet parameters**
    - Pellet radial velocity,  $v_r$
    - Pellet mass density,  $\rho_z$
    - Pellet radius,  $r_p$  (experimental limit for NSTX-U would be 1 mm. We fixed at this value)

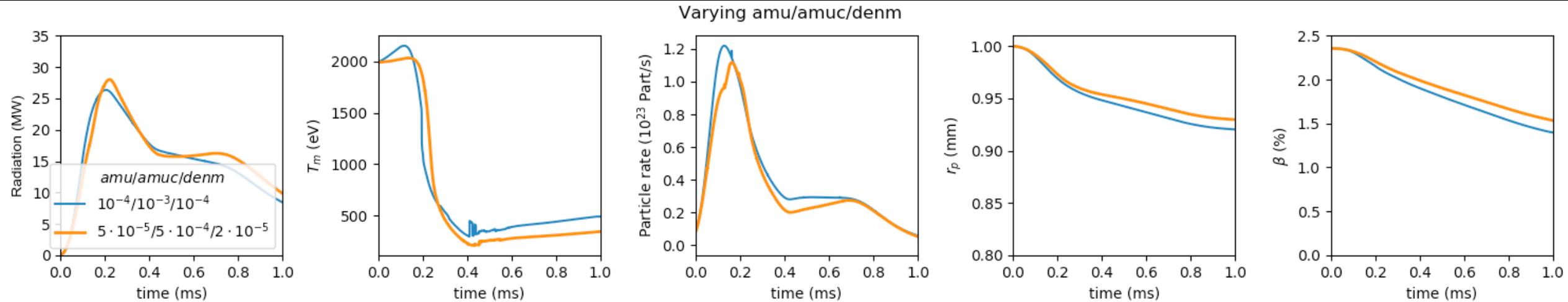
**We need first a clear picture on modelling parameters before moving to scan pellet parameters**

**In addition, scanning on different parameters can help clarifying the physics behind this process**



# NSTX-U: Scanning over modelling parameters

## Effect of viscosity ( $\mu, \mu_c$ ) and density diffusion (denm)



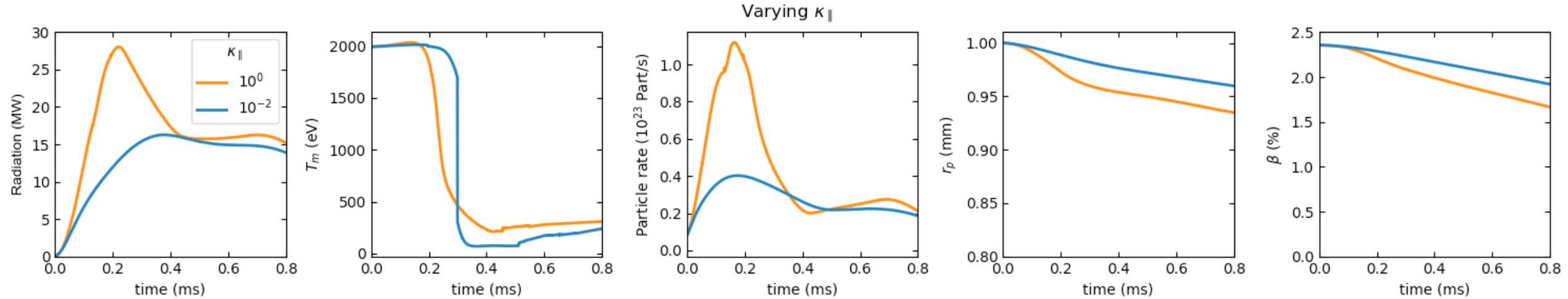
The **orange case** will be our reference case

- Having larger diffusion coefficients allow bigger time steps (0.5 blue and 0.2-0.25 orange)
- Central temperature can show some differences, but global quantities are similar.
- We can show that reducing even more this quantities does not produce further differences (in progress)



# NSTX-U: Scanning over modelling parameters

## Effect parallel thermal conductivity



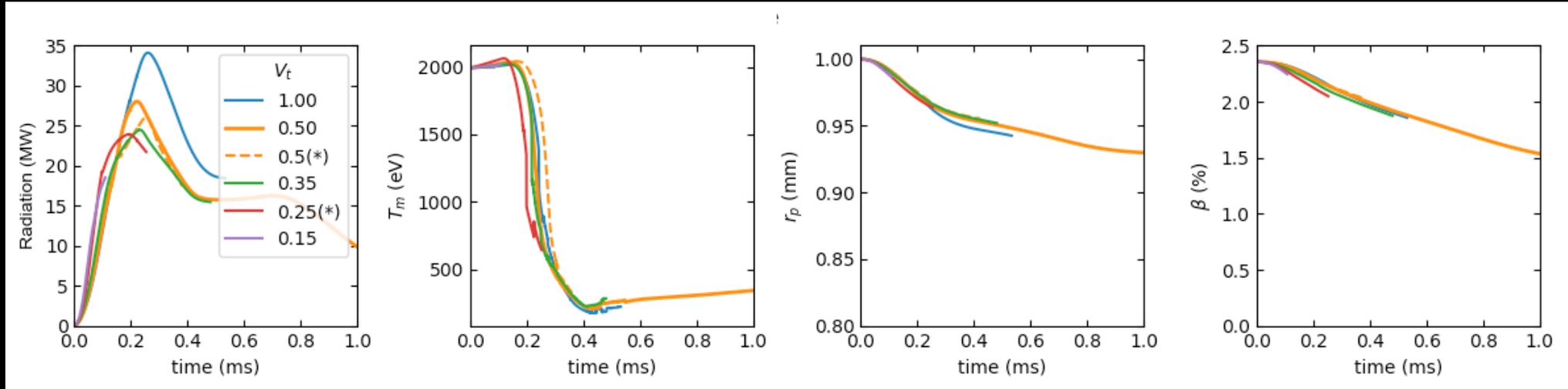
Parameter	value
$v_p$	1000 m/s
$V_p$	$50r_p$ ( $\sim 5$ cm)
$\kappa_{\perp}$	$2 \cdot 10^{-6}$
$\mu/\mu_c$	$5 \cdot 10^{-5}/5 \cdot 10^{-4}$

- $\kappa_{\parallel}$  has a strong role on pellet related quantities
- From the comparison with the AUG discharge,  $\kappa_{\parallel} = 1$  seems to be a fear value
- Larger  $\kappa_{\parallel}$  also requires smaller time steps
- In addition, very large  $\kappa_{\parallel}$  values can lead to anomalous perpendicular heat flux (if the mesh is not fine enough) \*
- In progress: explore larger  $\kappa_{\parallel}$



# NSTX-U: Scanning over modelling parameters

## Effect of pellet neutral cloud size



Parameter	value	Obs
$v_p$	1000 m/s	
$V_p$	$50r_p$ ( $\sim 5$ cm)	Case 0.5(*) has $25r_p$
$\kappa_{\parallel}/\kappa_{\perp}$	$\sim 10^6$	

- Case 0.25(\*) has a bit larger viscosity.
- **Almost everything looks similar, except the radiation for  $V_t = 1.00$  (a bit larger).**
- **Thus, the reference case is taken to be  $V_t = 0.50$  (16 planes) and  $V_p = 50r_p$ .**

Case	# planes	Smallest dt needed
<b>1.0</b>	12	0.15
<b>0.50</b>	16	0.20
<b>0.5(*)</b>	16	0.15
<b>0.35</b>	16	0.05
<b>0.25(*)</b>	32	< 0.1
<b>0.15</b>	32	< 0.02

**All the previous cases show an incomplete TQ**



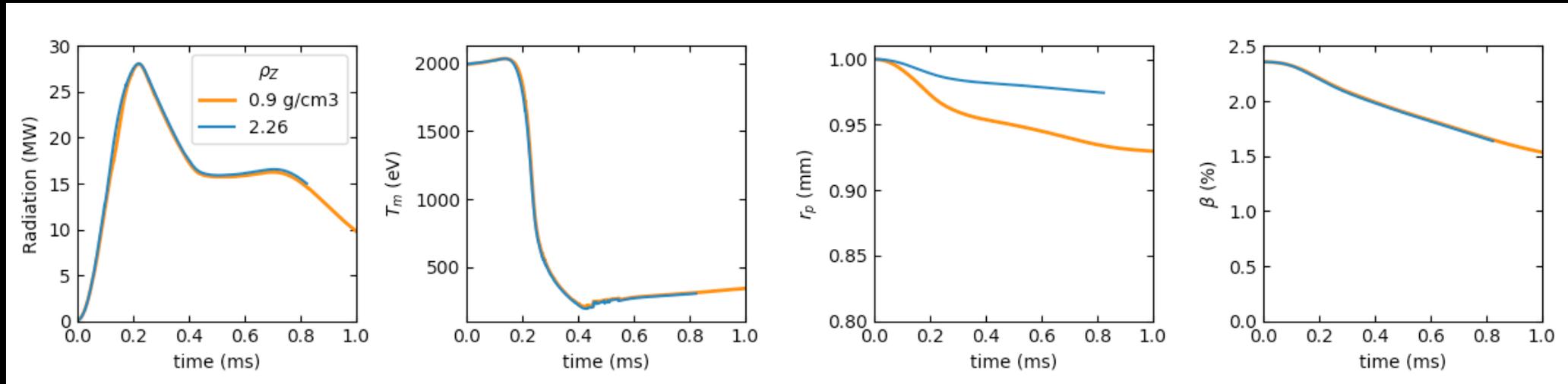
# NSTX-U: Scanning over pellet parameters

## Covering different pellet densities

There are different C materials: Candidate is vitreous carbon

We covered both ends

material	$\rho_Z$ (g/cm <sup>3</sup> )
Graphite	2.267
Vitreous	1.51
Sergeev*	0.9



Parameter	value
$v_p$	1000 m/s
$V_t/V_p$	0.5 / $50r_p$
$\kappa_{  }/\kappa_{\perp}$	$\sim 10^6$

Results are almost identical

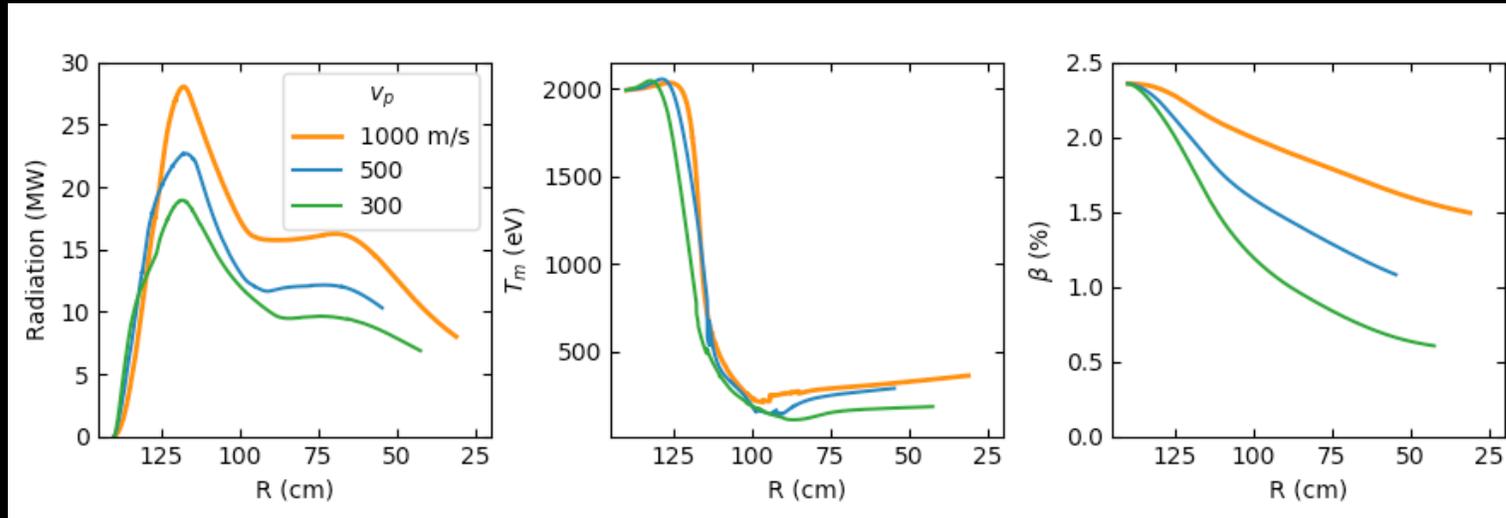
Pellet radius is different because of the different pellet densities but the same ablation rate.



# NSTX-U: Scanning over pellet parameters

## Effect of different pellet velocities

- The reference case (orange curve) is not enough to produce a complete TQ since  $\beta$  dropped from 2.5% to 1.5%
- We ran a cases with pellet velocities of 500 m/s and 300 m/s.
- In this case figures are shown as a function of the radial position (not time as previous cases).

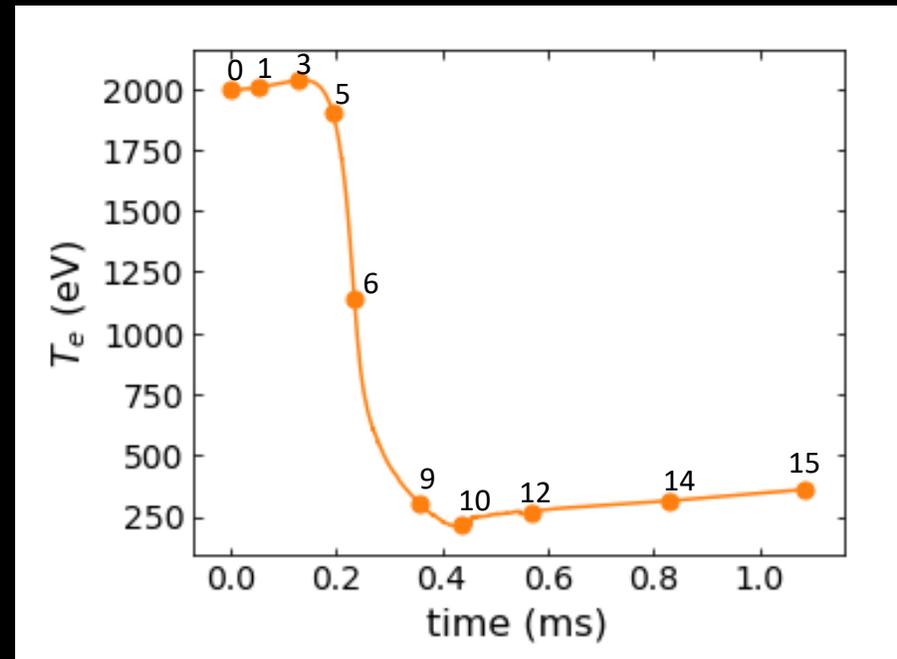


- $\beta$  drop is very sensitive to the pellet velocity

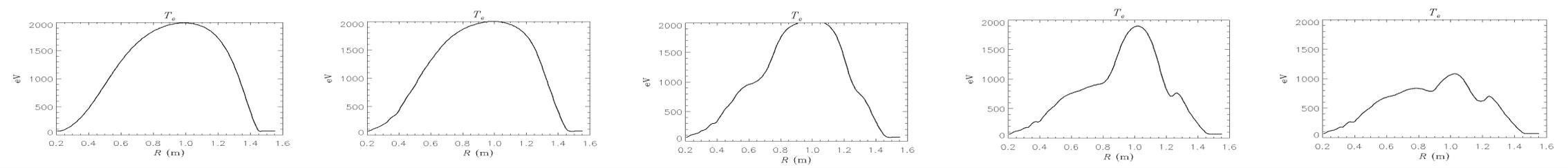
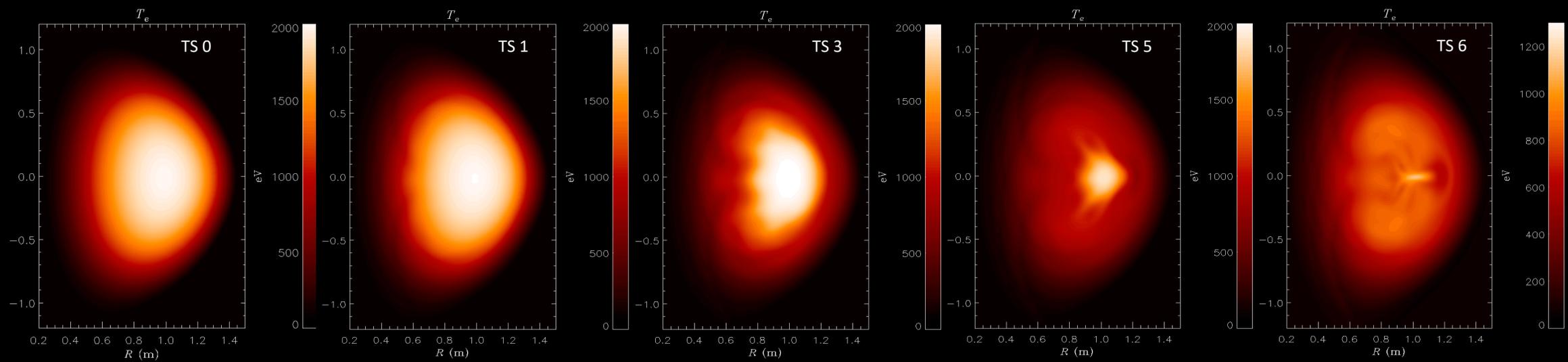
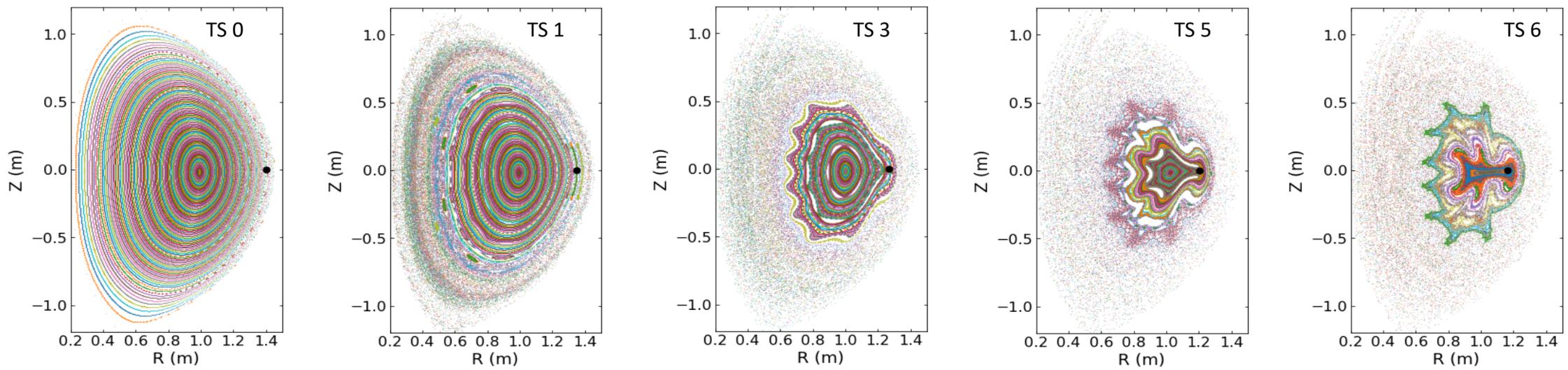


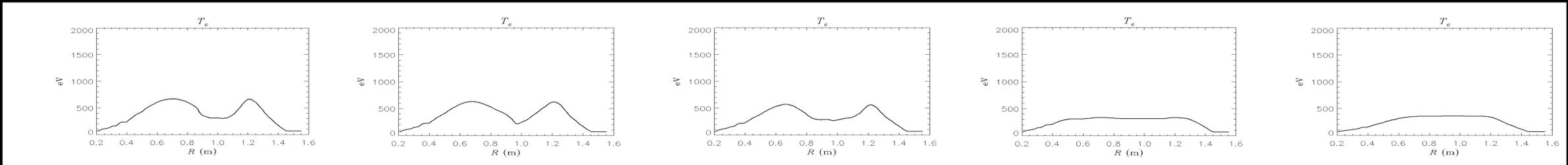
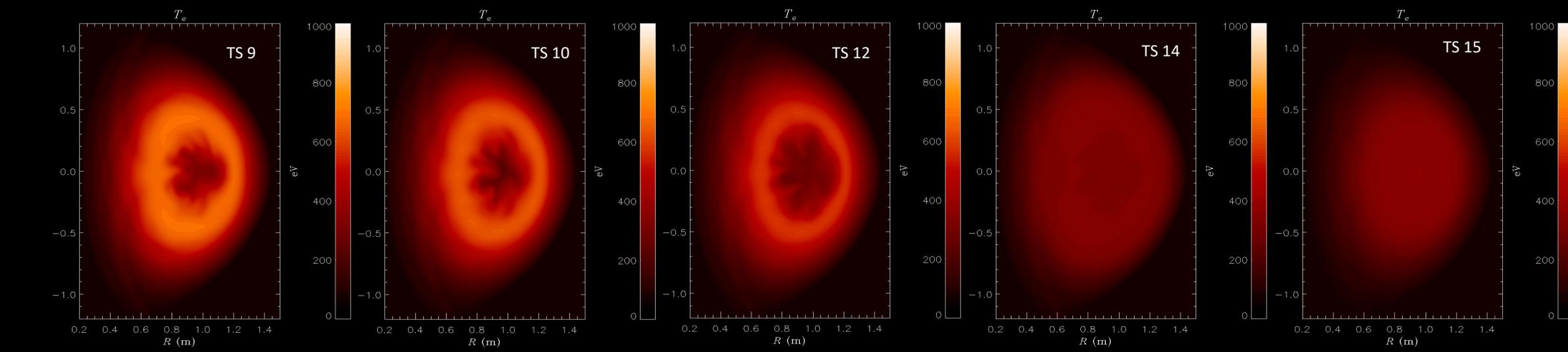
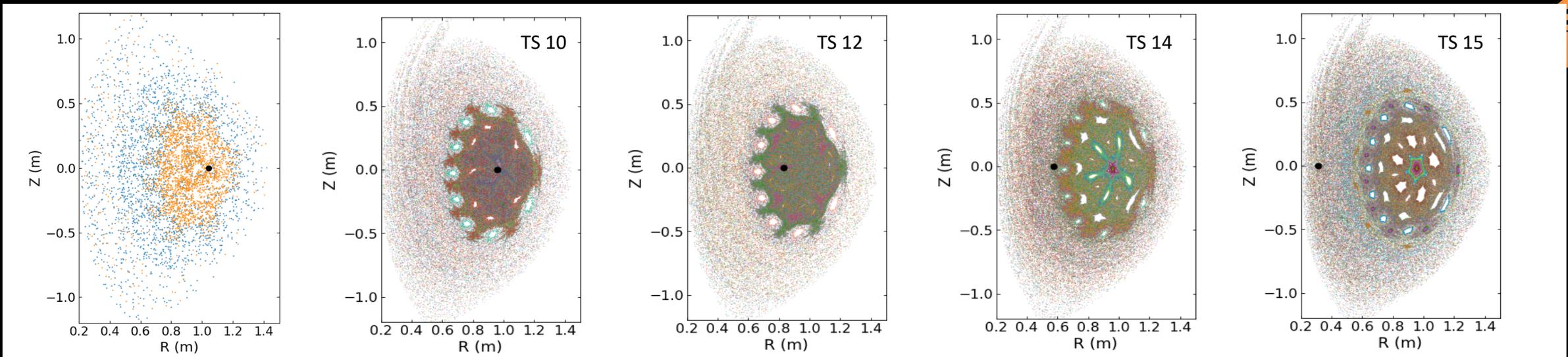
# NSTX-U: Understanding the TQ

## Central temperature as a function of time



- In the next slides we will show Poincare plots and temperature distribution at all these timeslices.







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# NSTX-U: Summary

- We incorporated a C-ablation model in M3D-C1
  - The model was tested in an AUG discharge in which data exists getting a very good agreement
- We have carried out a convergence study for an NSTX-U discharge
  - We evaluated the sensitivity of different parameters
  - Parallel heat flux and pellet velocity are the most important parameters to produce a TQ
  - We showed that central temperature cools down before the pellet reaches it

## Still in progress

- Larger  $\kappa_{\parallel}$  (to the mesh limit)
- Explain the central cooling mechanism
  - We are analyzing each term in the temperature equation separately
- Compute the Current Quench for selected case(s)

## Moving forward (\*)

- Shell pellet. Start ablating inside the  $q=2$ 
  - Our equilibrium has  $q \gtrsim 2$  at the core
  - Search for a new equilibrium with  $q < 2$
- Explore other pellet materials: B, Boron Nitride, Be, W.
- Simulate an ITER pellet injection





# KPRAD Coupling in M3D-C1

$$\frac{\partial n_i}{\partial t} + \nabla \cdot (n_i \mathbf{v}) = D \nabla^2 n_i + \sigma_i \quad (\text{idem } n_Z^{(j)})$$

$$\rho \left( \frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} \right) = \mathbf{J} \times \mathbf{B} - \nabla p - \nabla \cdot \Pi - \bar{\omega} \mathbf{v}$$

$$\rho = m_i n_i + \sum_{j=1}^Z m_Z n_Z^{(j)} \quad \bar{\omega} = m_i \sigma_i + \sum_{j=1}^Z m_Z \sigma_Z^{(j)}$$

$$\mathbf{E} = \eta \mathbf{J} - \mathbf{v} \times \mathbf{B}$$

$$n_e \left[ \frac{\partial T_e}{\partial t} + \mathbf{v} \cdot \nabla T_e + (\Gamma - 1) T_e \nabla \cdot \mathbf{v} \right] + T_e (D \nabla^2 n_e + \sigma_e) = (\Gamma - 1) [\eta \mathbf{J}]^2 - \nabla \cdot \mathbf{q}_e + Q_e + Q_\Delta - \Pi_e : \nabla \mathbf{v}$$

$$n_* \left[ \frac{\partial T_i}{\partial t} + \mathbf{v} \cdot \nabla T_i + (\Gamma - 1) T_i \nabla \cdot \mathbf{v} \right] + T_i (D \nabla^2 n_* + \sigma_*) = (\Gamma - 1) \left[ -\nabla \cdot \mathbf{q}_* + Q_* - Q_\Delta - \Pi_* : \nabla \mathbf{v} + \frac{1}{2} \bar{\omega} v^2 \right]$$

$Q_{e,*}$  is the radiation source. It includes line radiation, Bremsstrahlung, recombination.



# Large density diffusion can increase the central temperature at the beginning

At the **beginning** and at the **center**, we have

- $\sigma_e = 0$  (no sources)
- $V=0$  (no rotation)
- heat flux is small (equil) and radiation should be small:  $q=0, Q=0$
- Ohmic heating should be small:  $\eta J = 0$

So, initially at the plasma center the equations reduces to

$$\frac{\partial n_e}{\partial t} = D \nabla^2 n_e$$

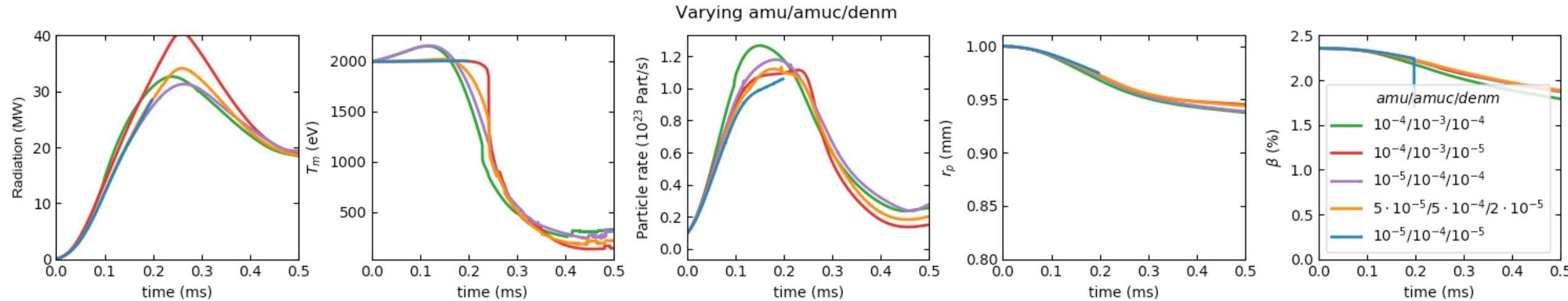
$$n_e \left[ \frac{\partial T_e}{\partial t} \right] + T_e (D \nabla^2 n_e) = 0$$

$\nabla^2 n_e$  is basically negative: that is why the density decreases, but that is also why the temperature increases



# NSTX-U: Scanning over modelling & other parameters

## Effect of viscosity ( $\mu, \mu_c$ ) and density diffusion (denm)



- Large density diffusion increases the central temperature
- Having higher diffusion coefficients allow larger time steps
- But also the central temperature can differ about 150 eV after the temperature fall

**Orange case** will be our reference case.

$\mu/\mu_c/\text{denm}$	$5 \cdot 10^{-5}/5 \cdot 10^{-4}/2 \cdot 10^{-4}$
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Case	Smallest dt needed
green	1.00
red	0.20
violet	0.30
orange	0.10
blue	0.02



# Case $v_p = 300$ m/s

